

Protection of timber structures – start time of charring and failure time

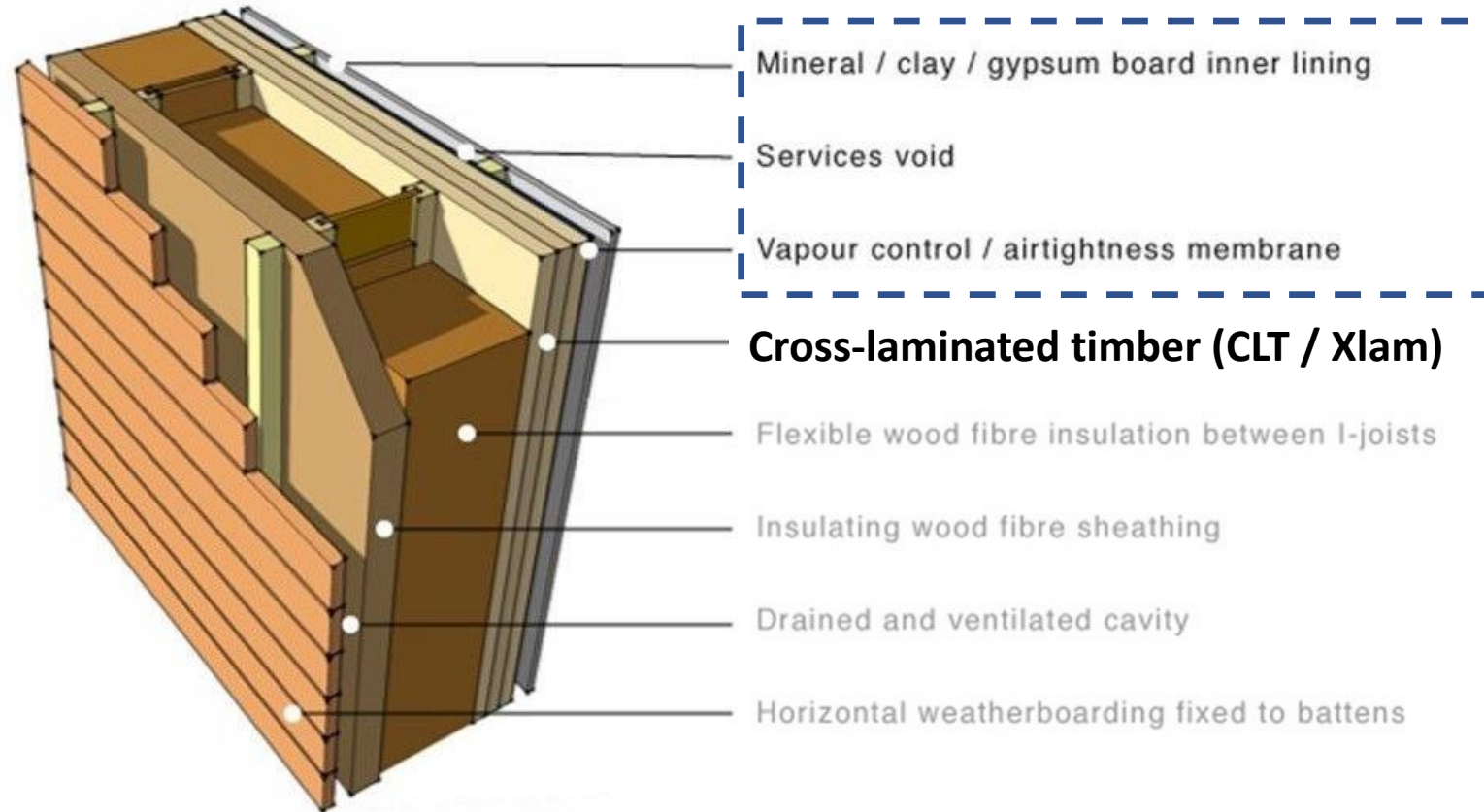
Alar Just

Tallinn University of Technology

RISE Research Institutes of
Sweden

27.09.2019

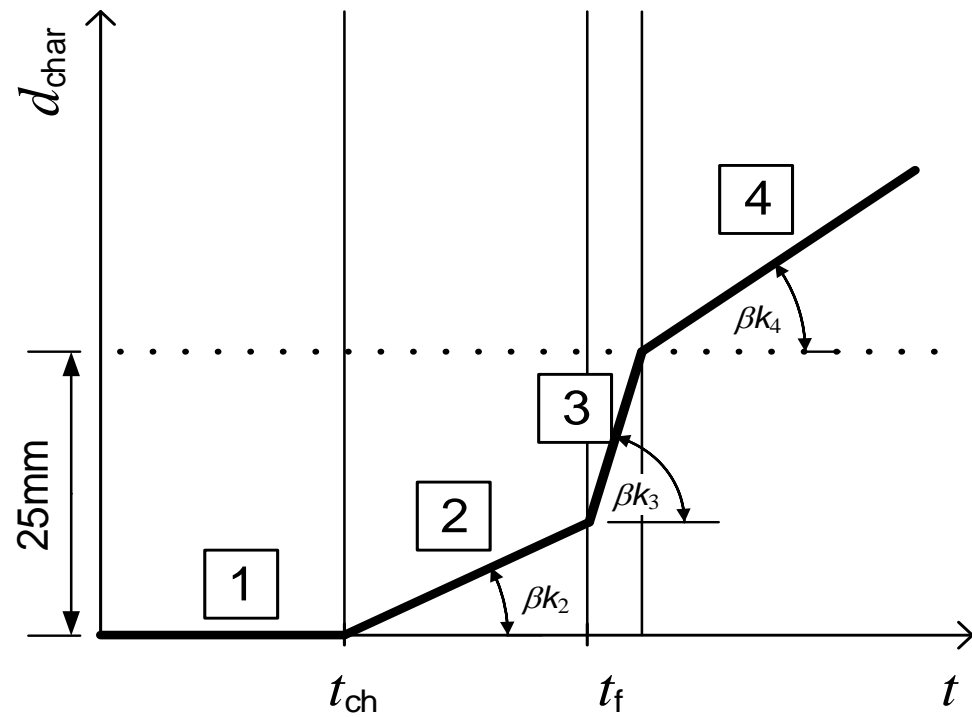
External wall with CLT load-bearing core



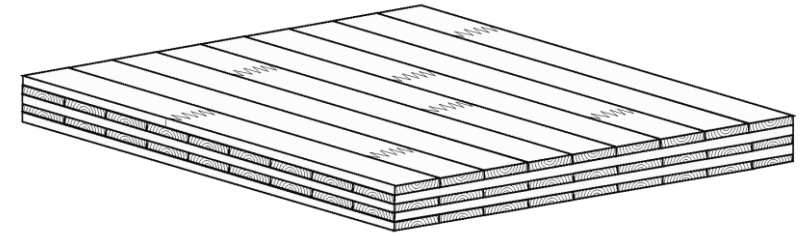
Fire
protection
system

Photo source: GreenSpec UK

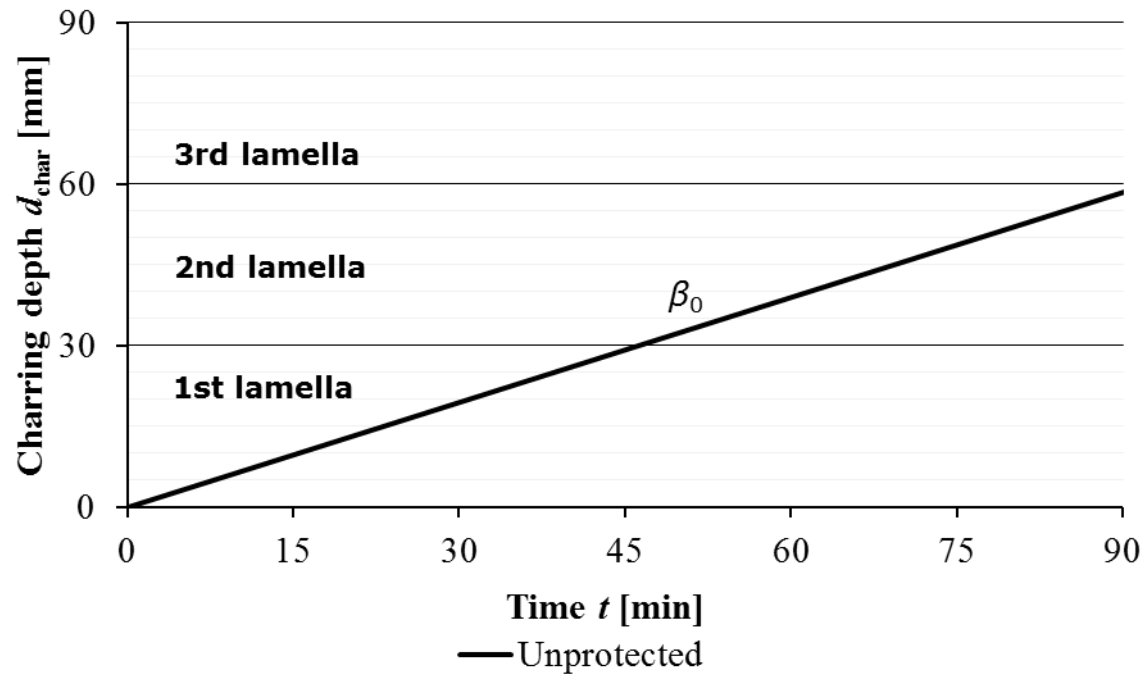
Charring of initially protected timber structures



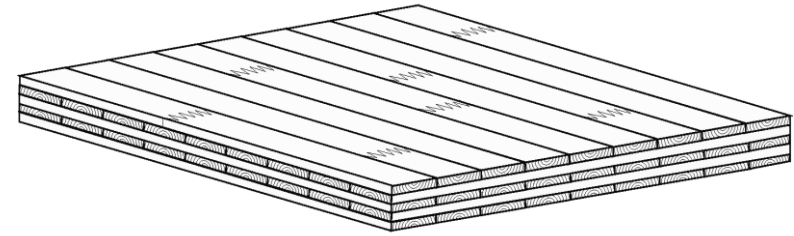
Charring of CLT: Adhesive behaviour



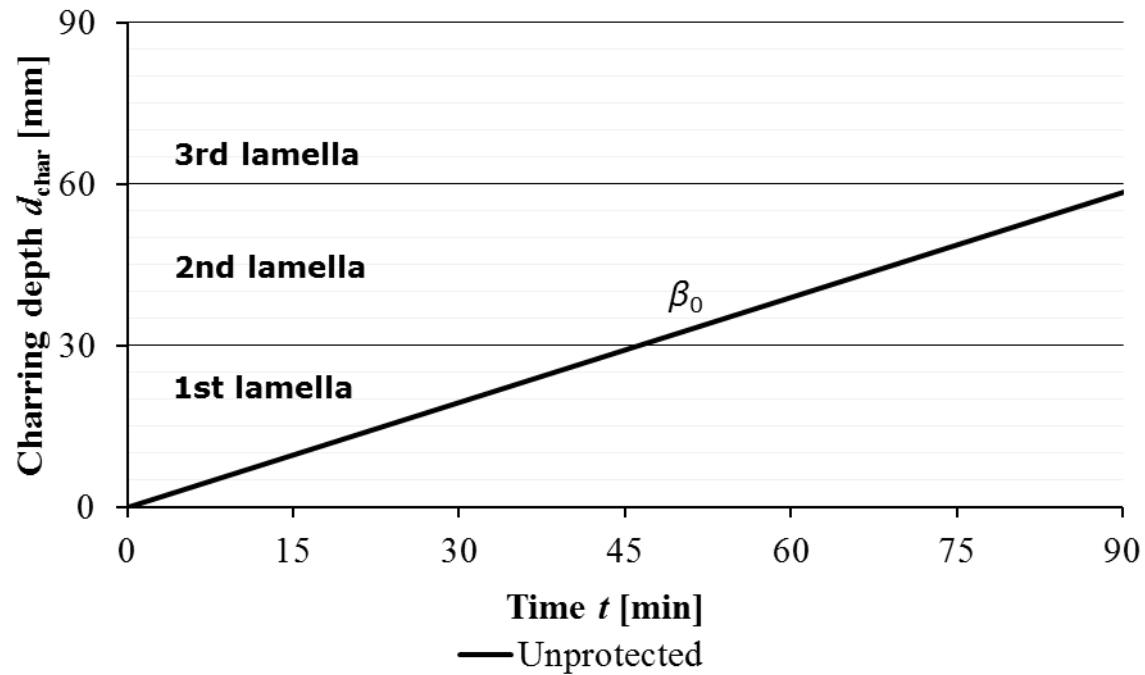
Heat-resistant adhesive



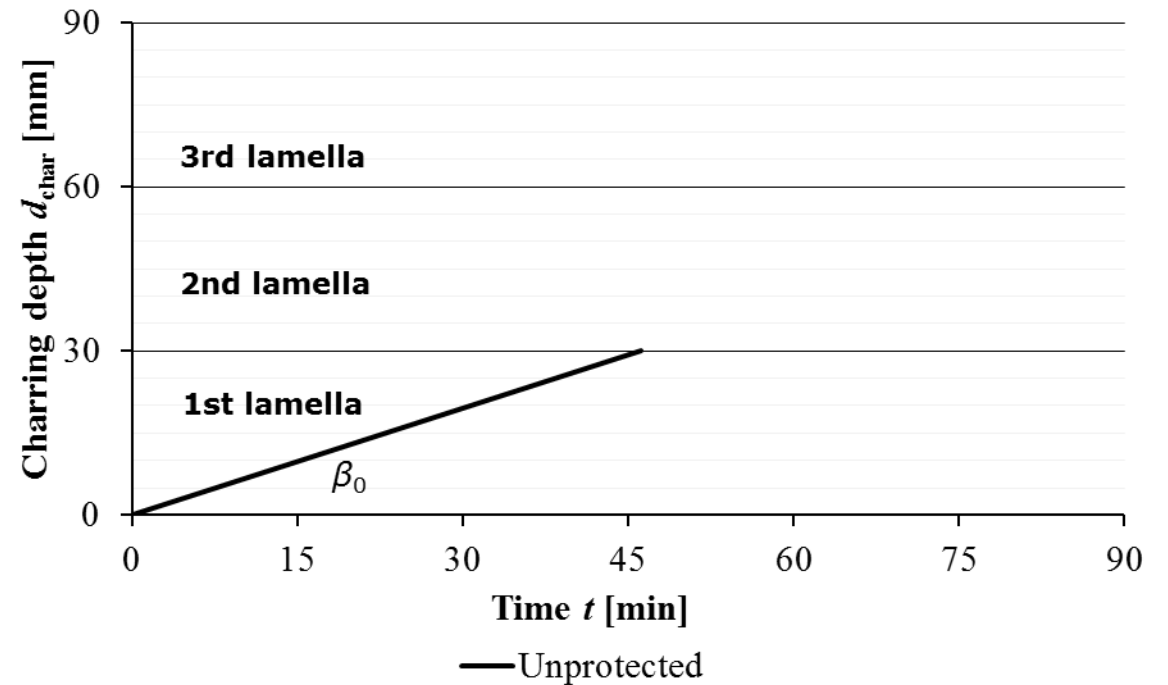
Charring of CLT: Adhesive behaviour



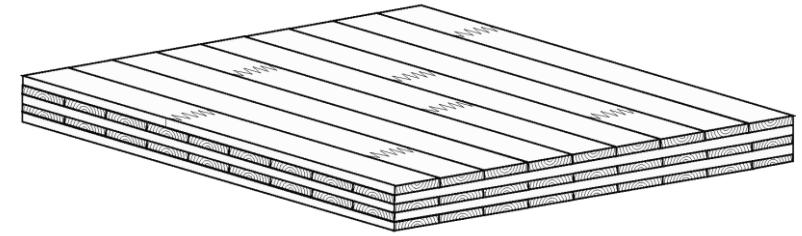
Heat-resistant adhesive



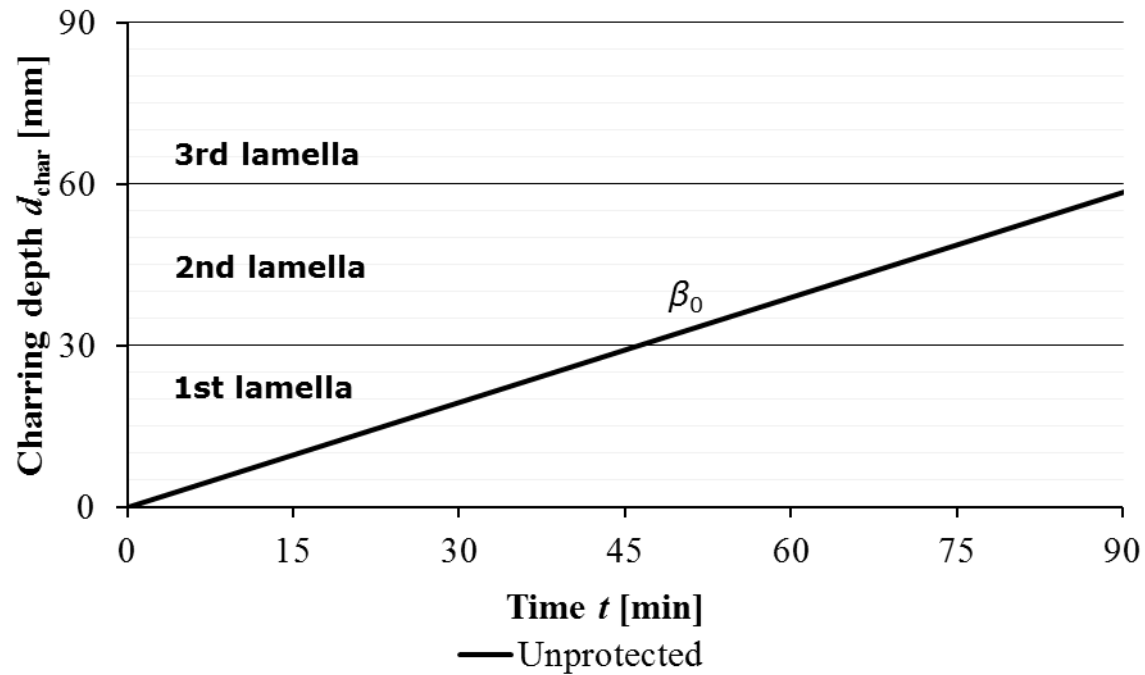
Non-heat-resistant adhesive



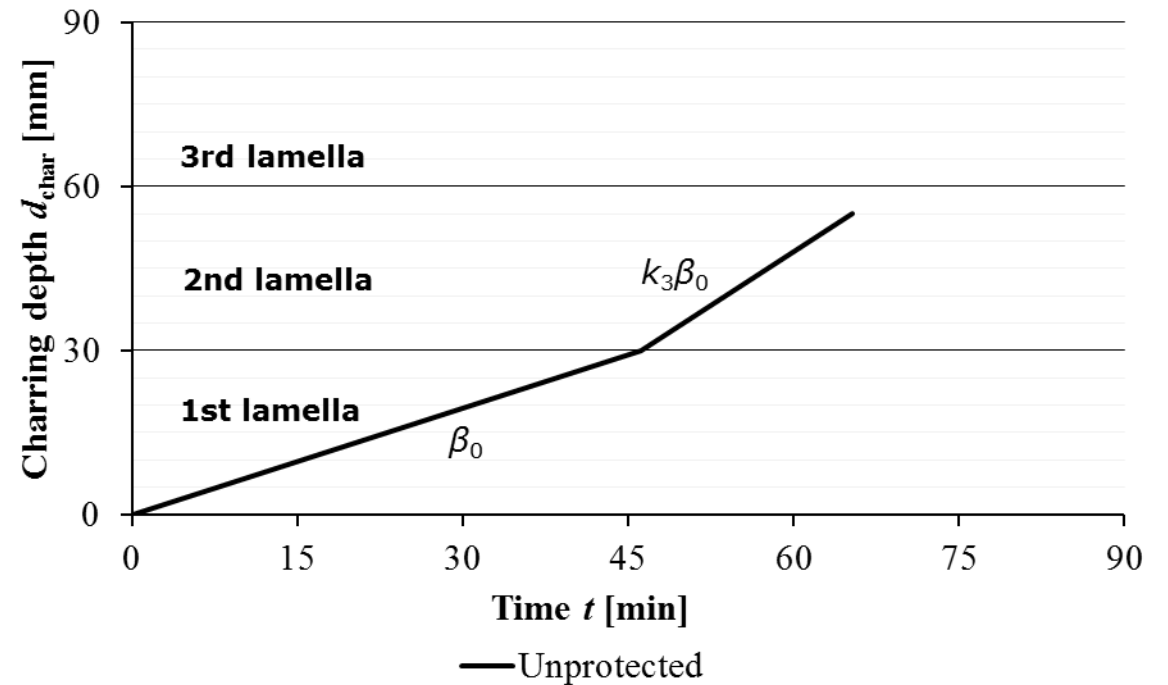
Charring of CLT: Adhesive behaviour



Heat-resistant adhesive



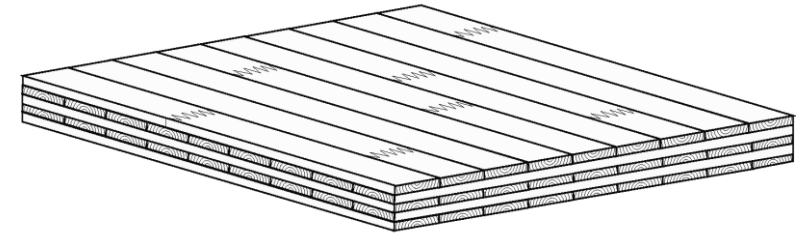
Non-heat-resistant adhesive



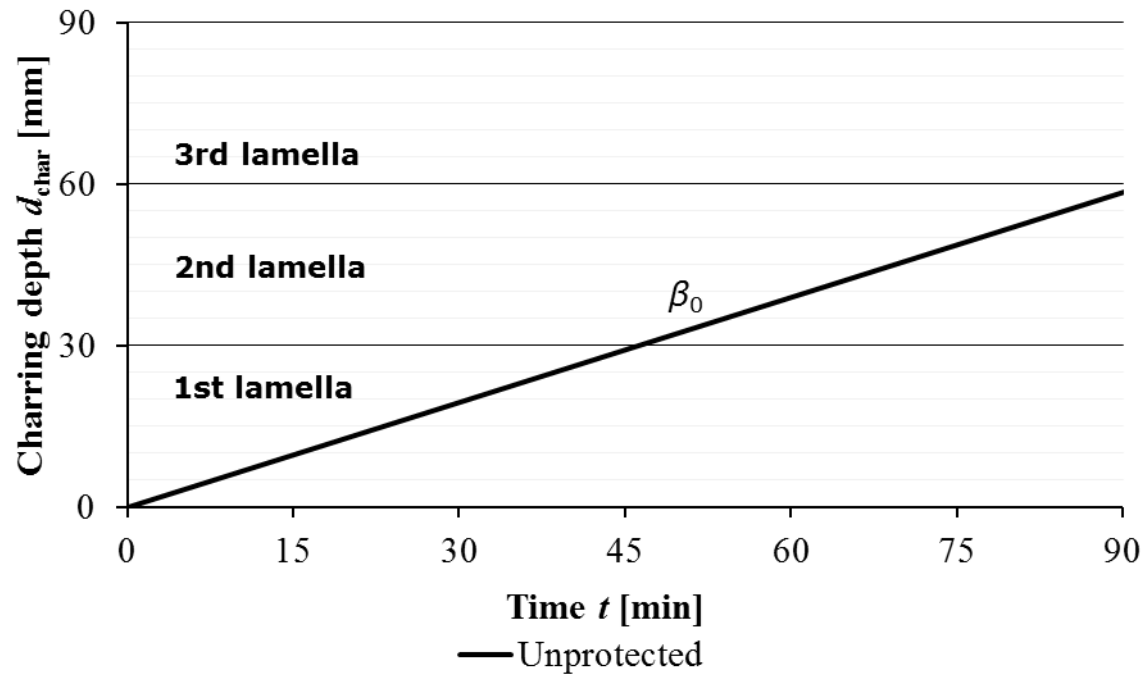
Non-heat-resistant adhesive Falling off of charred lamellas



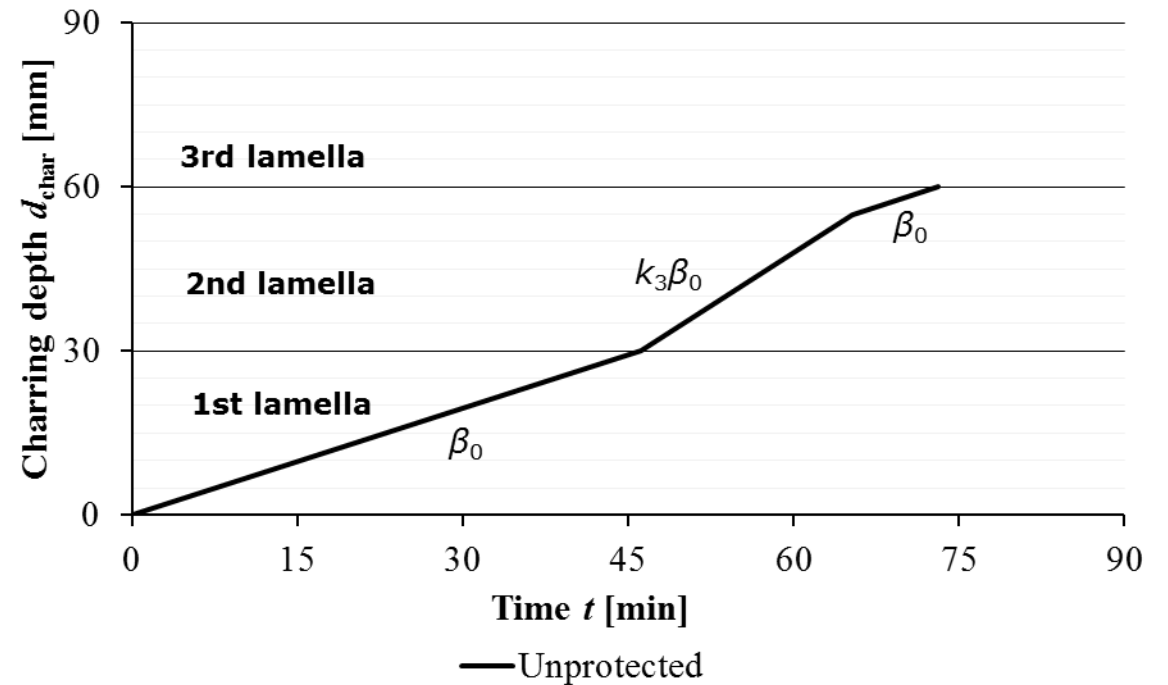
Charring of CLT: Adhesive behaviour



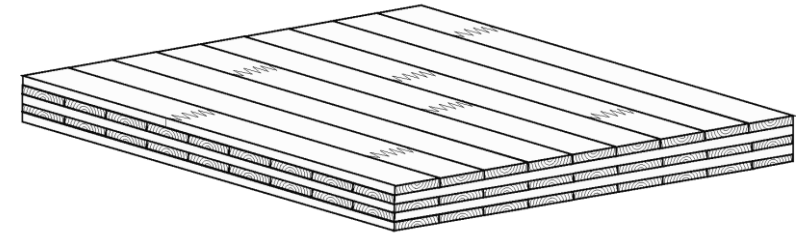
Heat-resistant adhesive



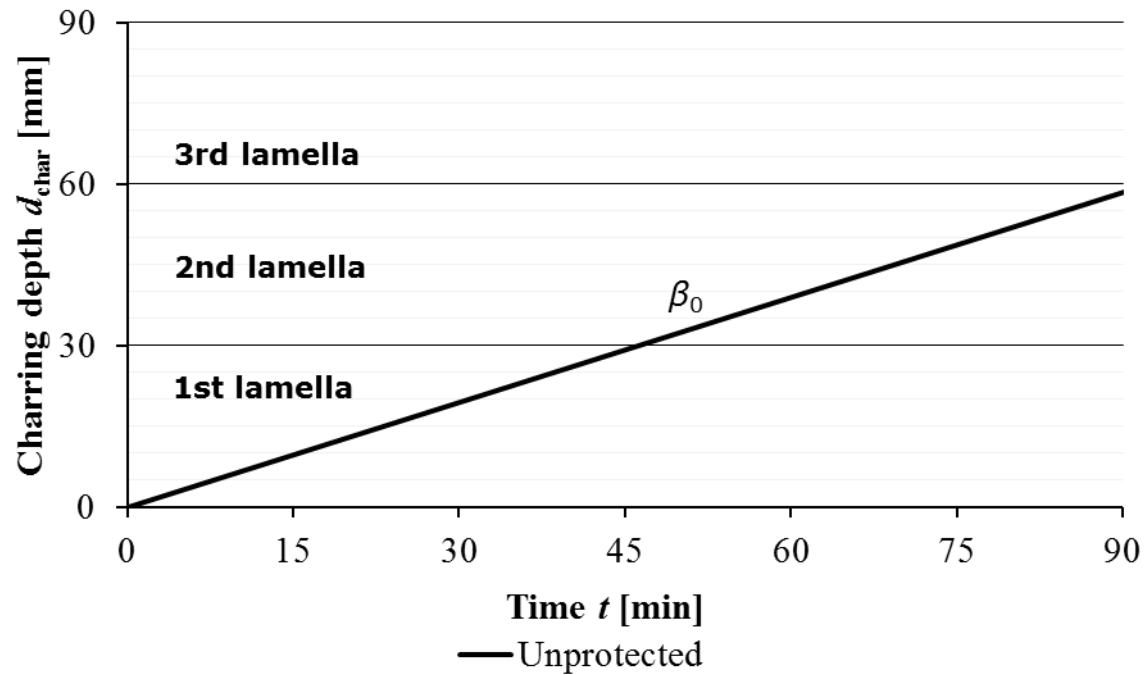
Non-heat-resistant adhesive



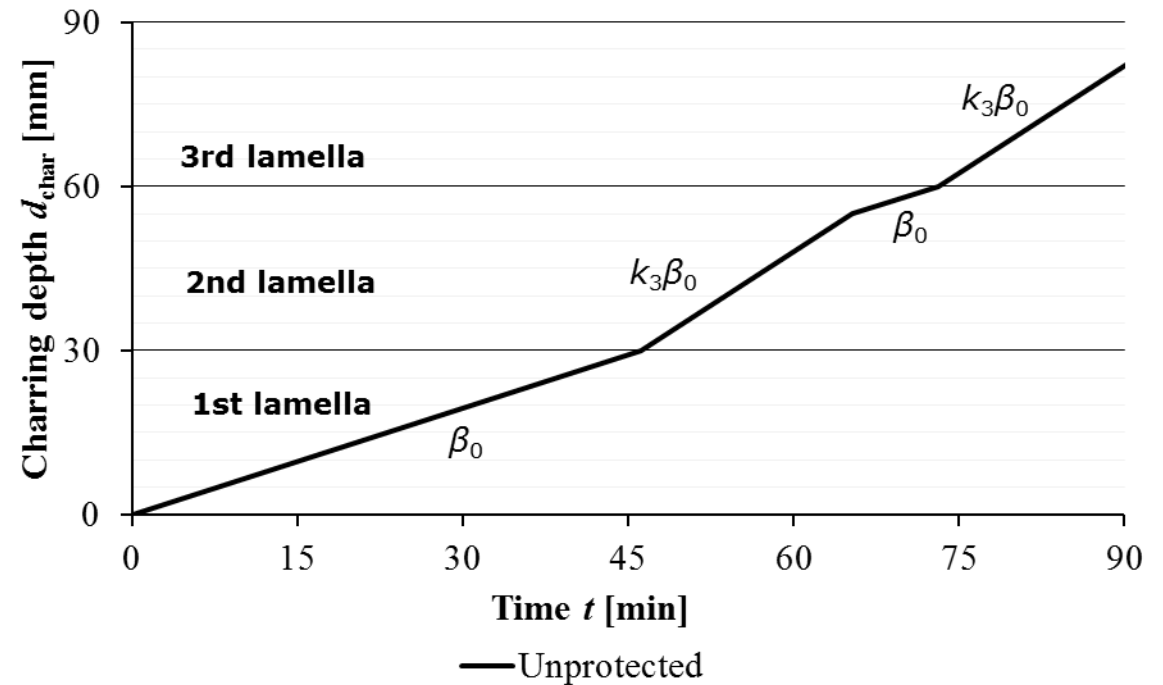
Charring of CLT: Adhesive behaviour



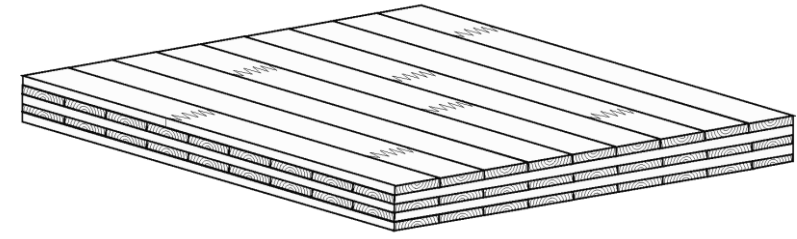
Heat-resistant adhesive



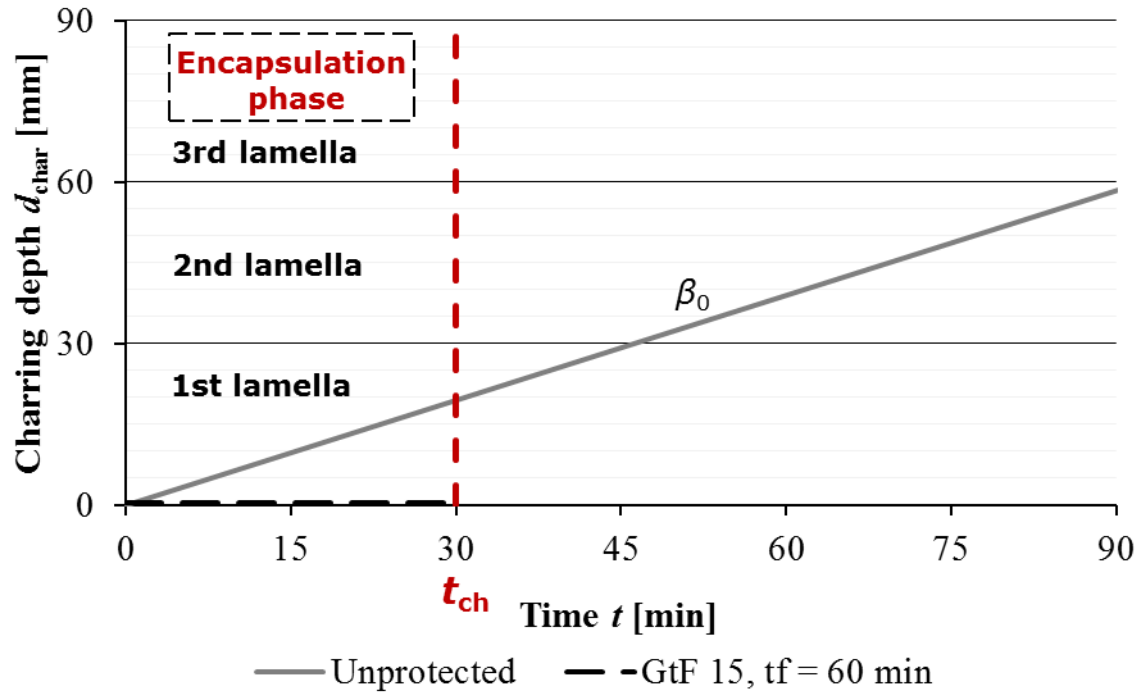
Non-heat-resistant adhesive



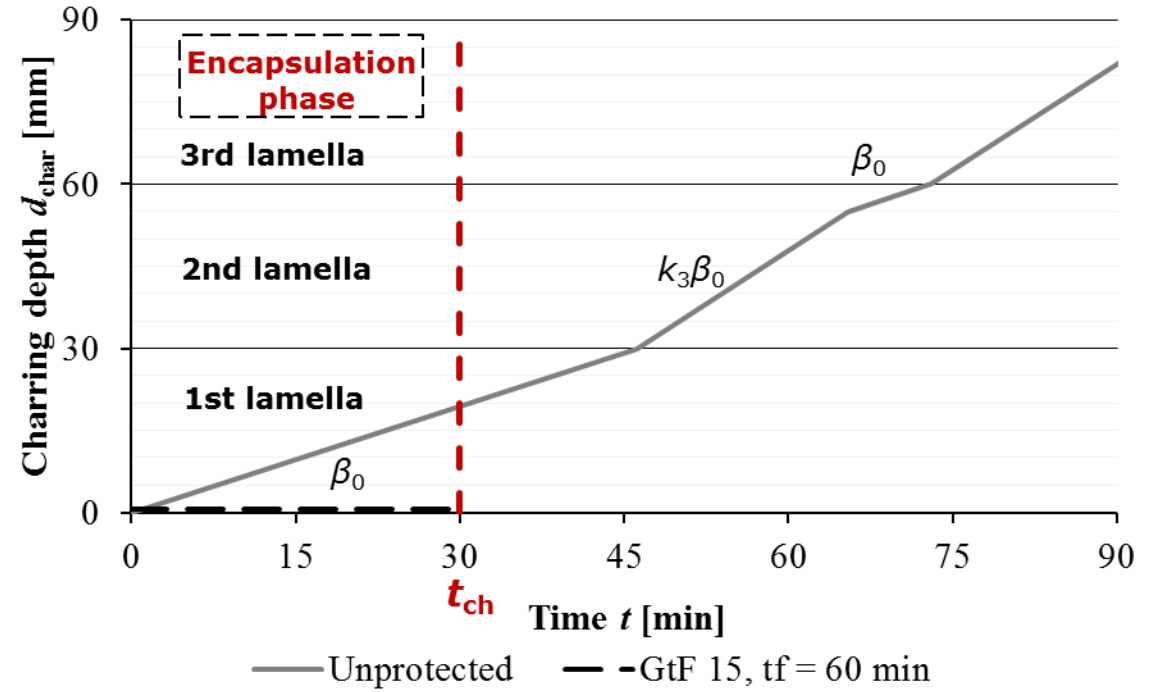
Charring of CLT: Charring phases



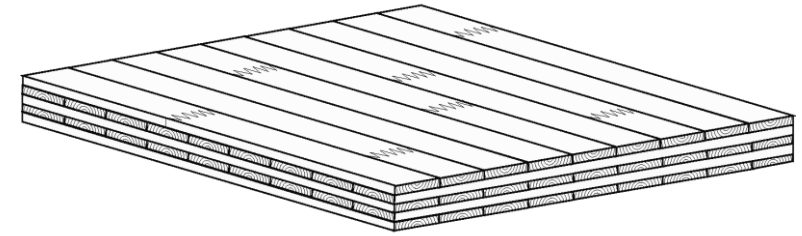
Heat-resistant adhesive



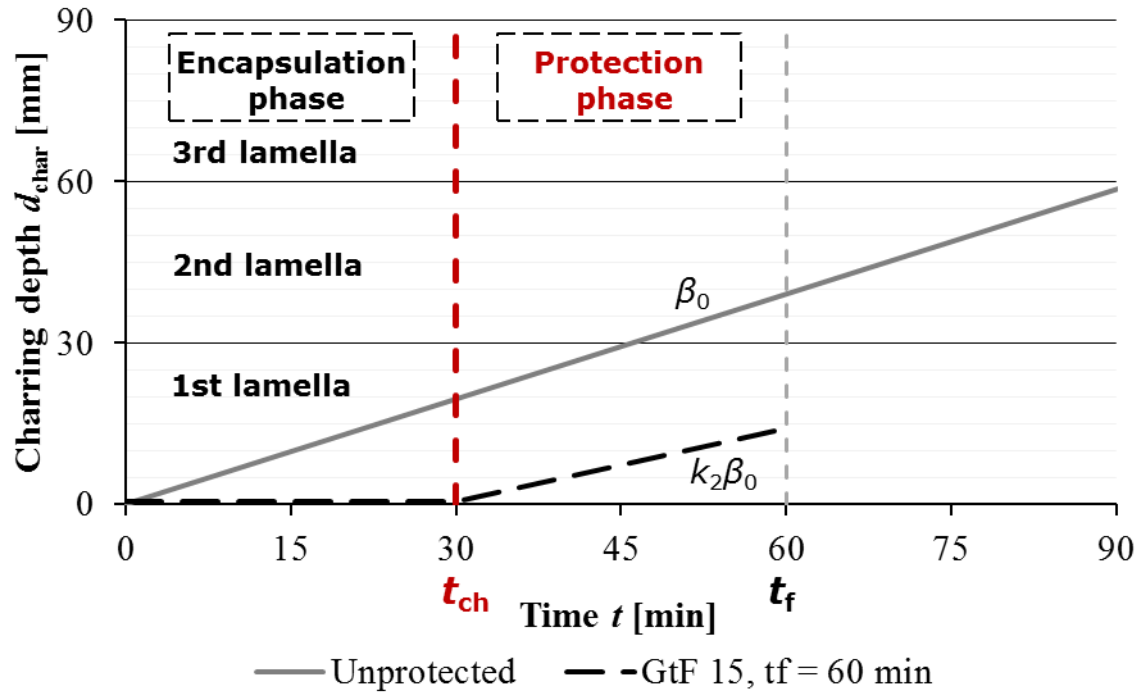
Non-heat-resistant adhesive



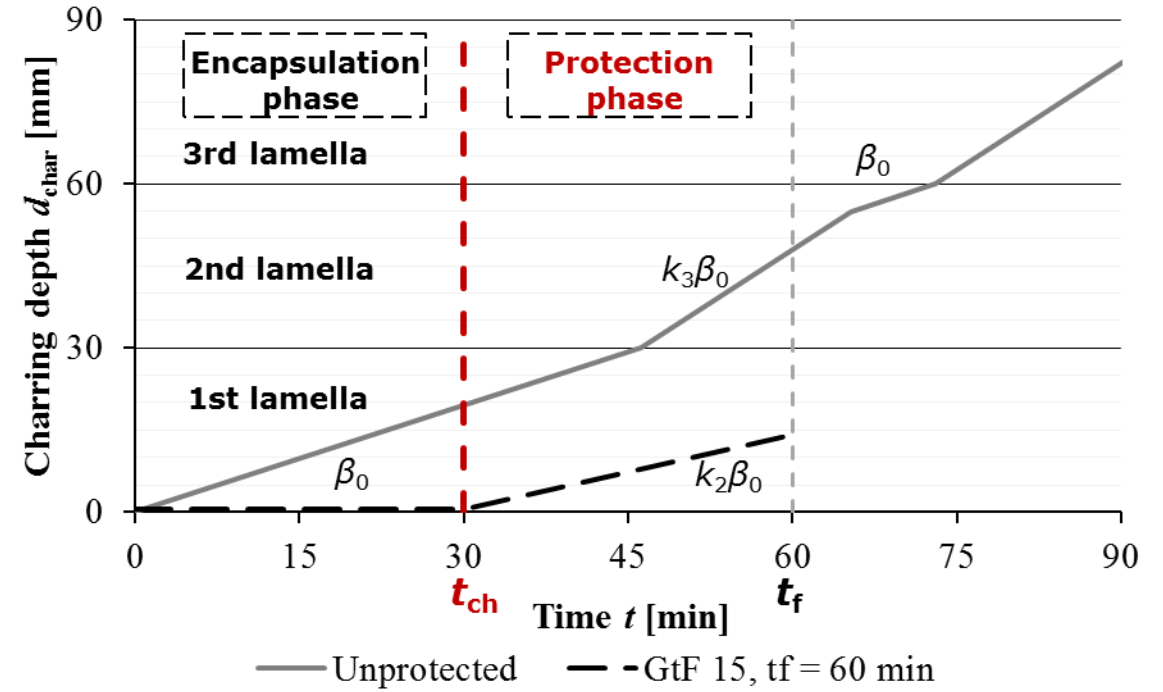
Charring of CLT: Charring phases



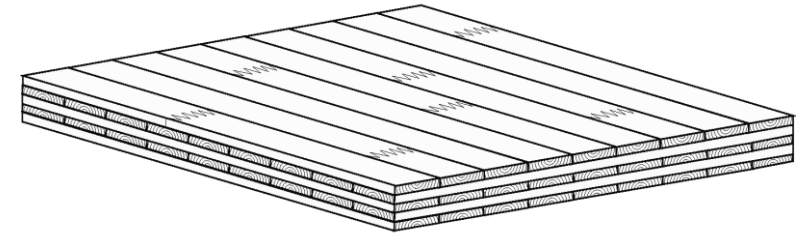
Heat-resistant adhesive



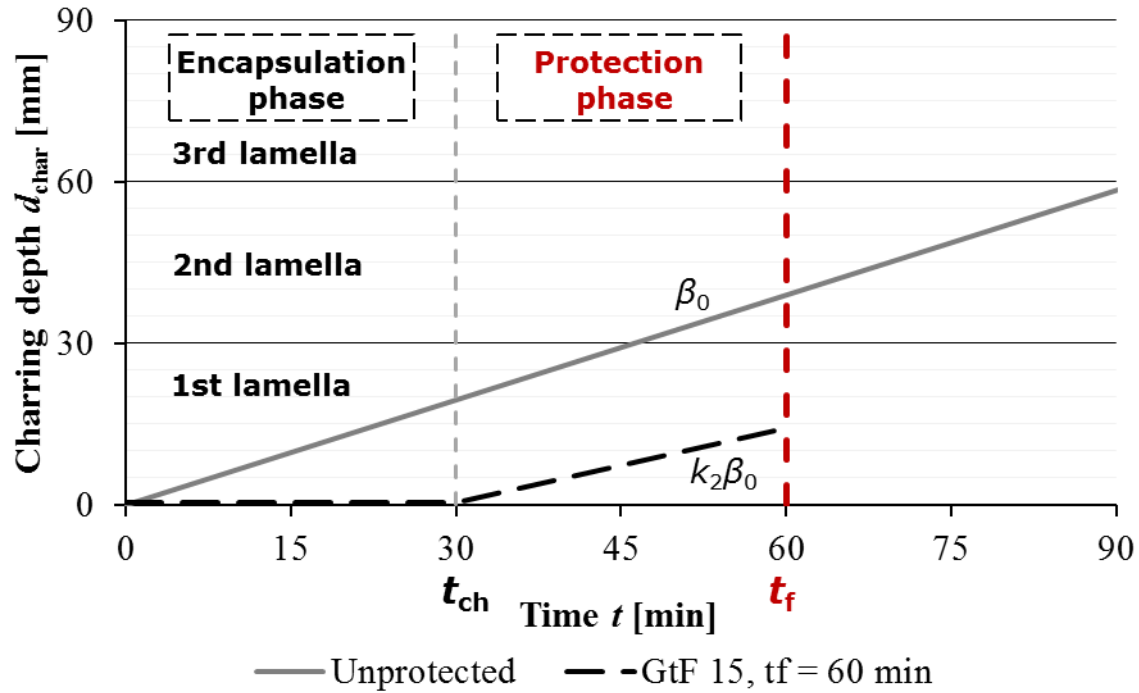
Non-heat-resistant adhesive



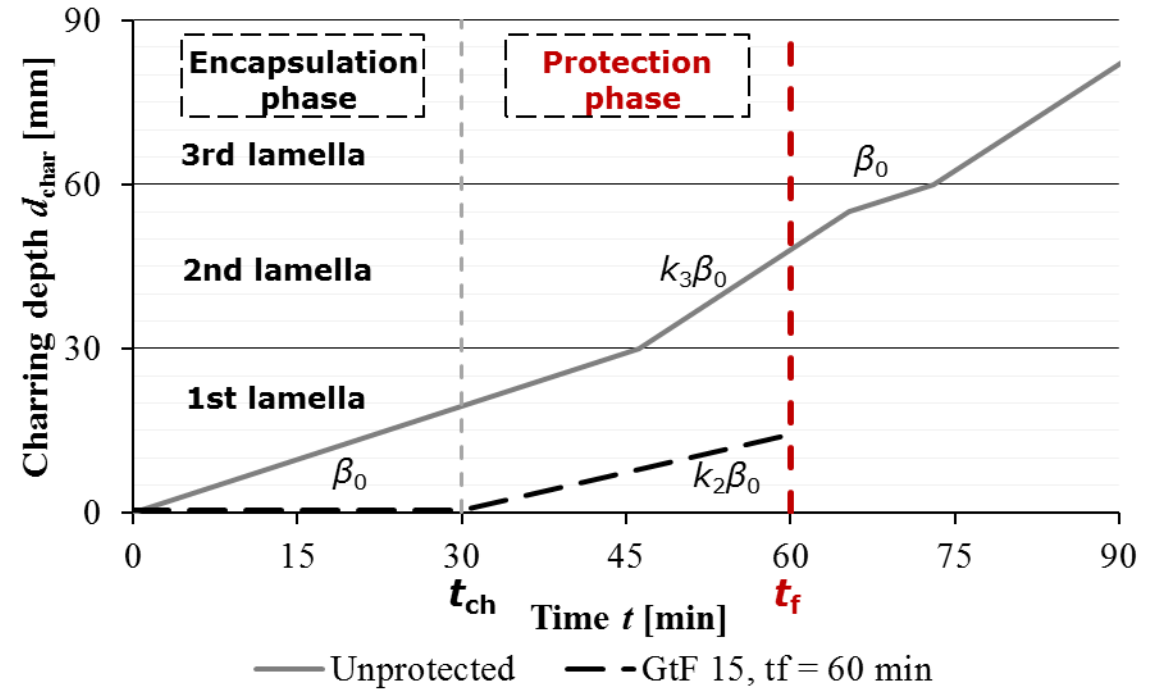
Charring of CLT: Charring phases



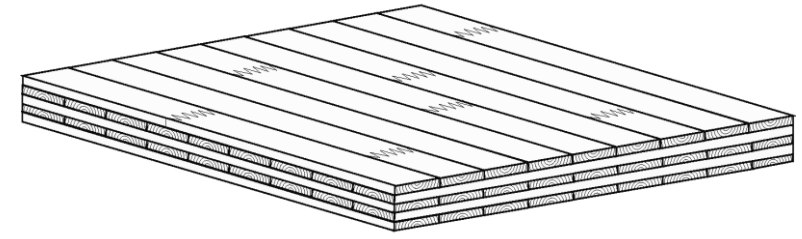
Heat-resistant adhesive



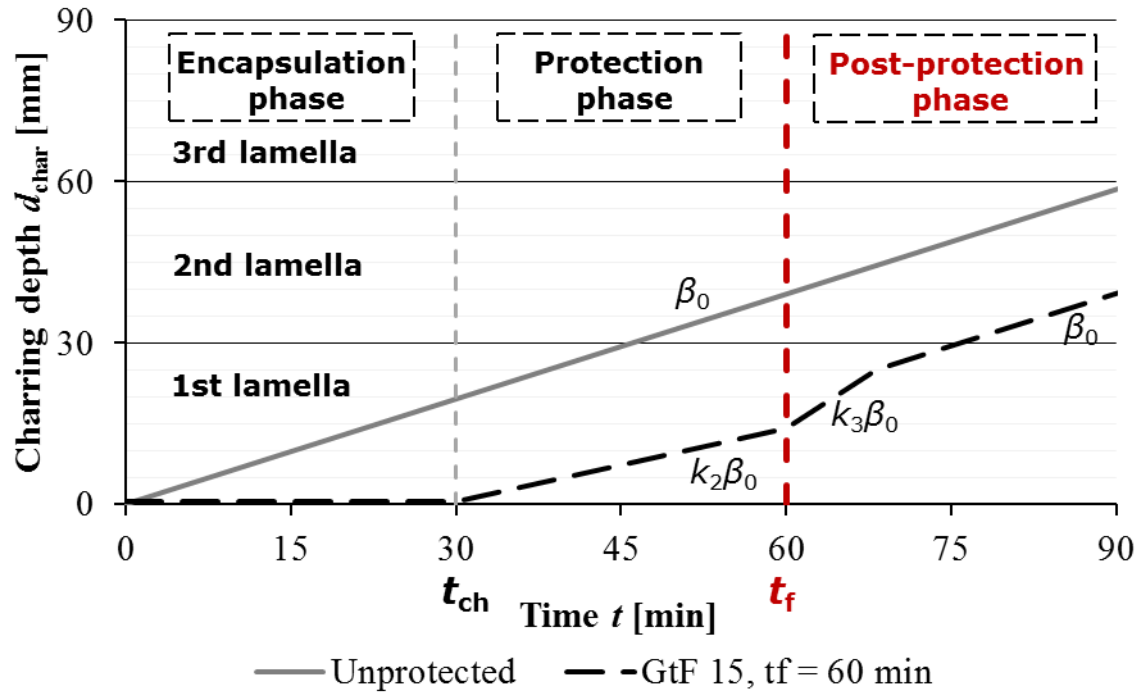
Non-heat-resistant adhesive



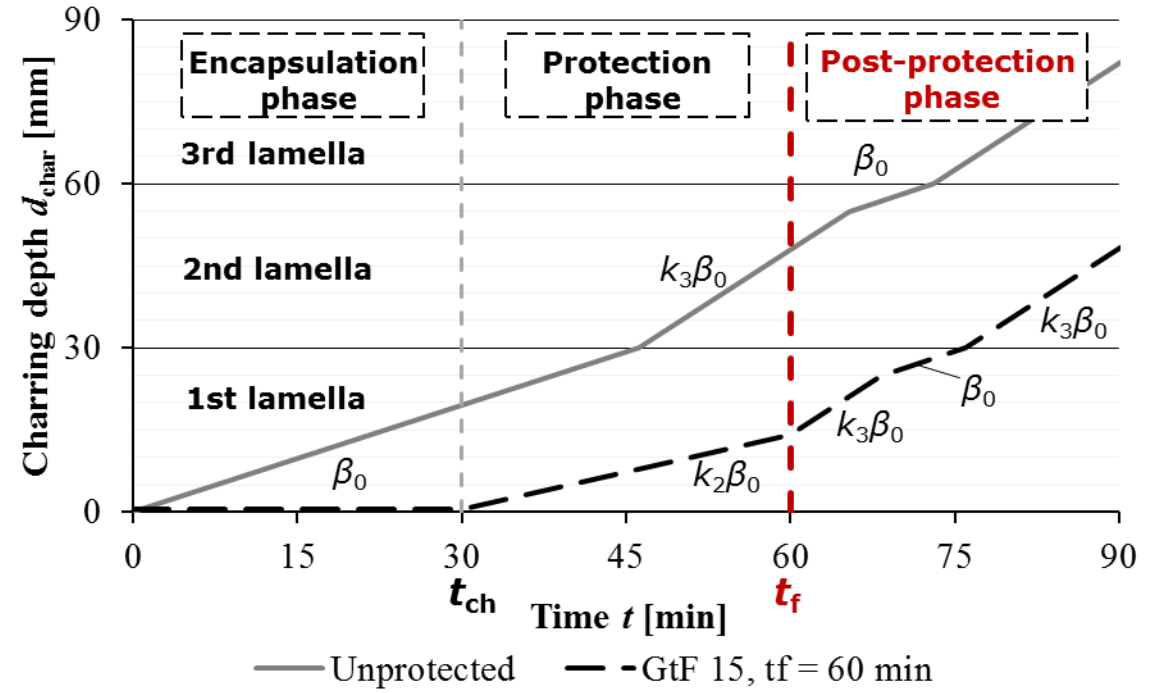
Charring of CLT: Charring phases



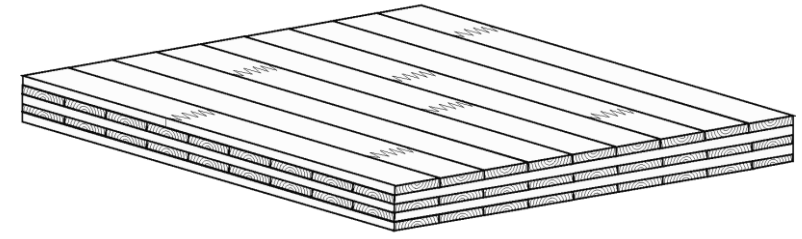
Heat-resistant adhesive



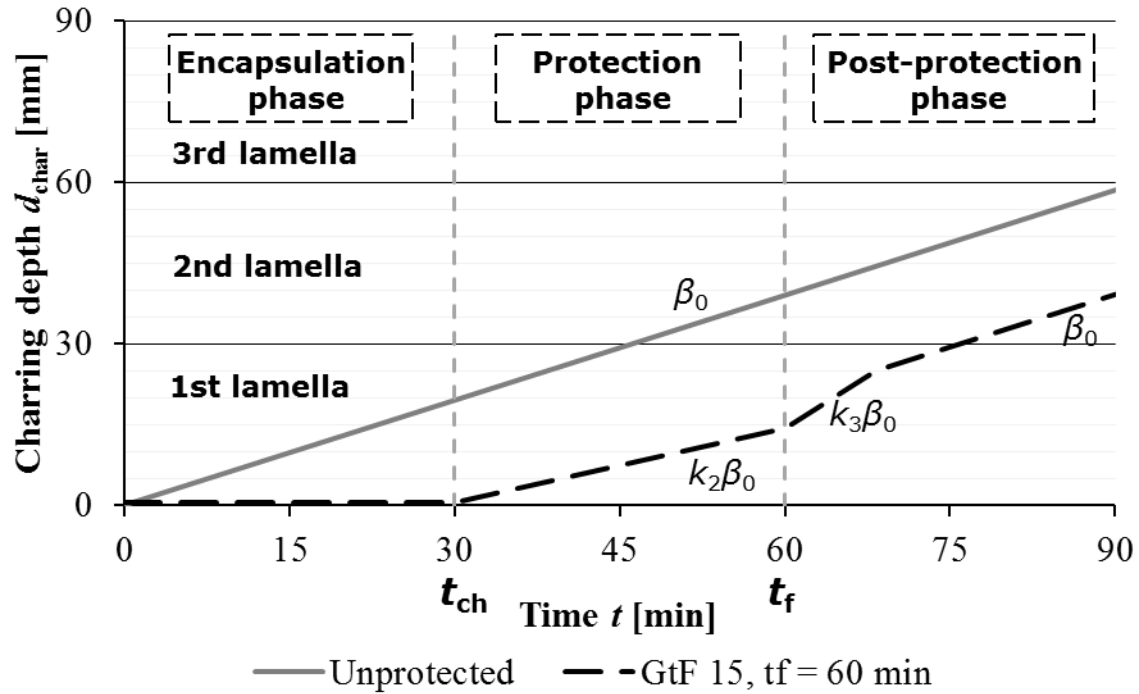
Non-heat-resistant adhesive



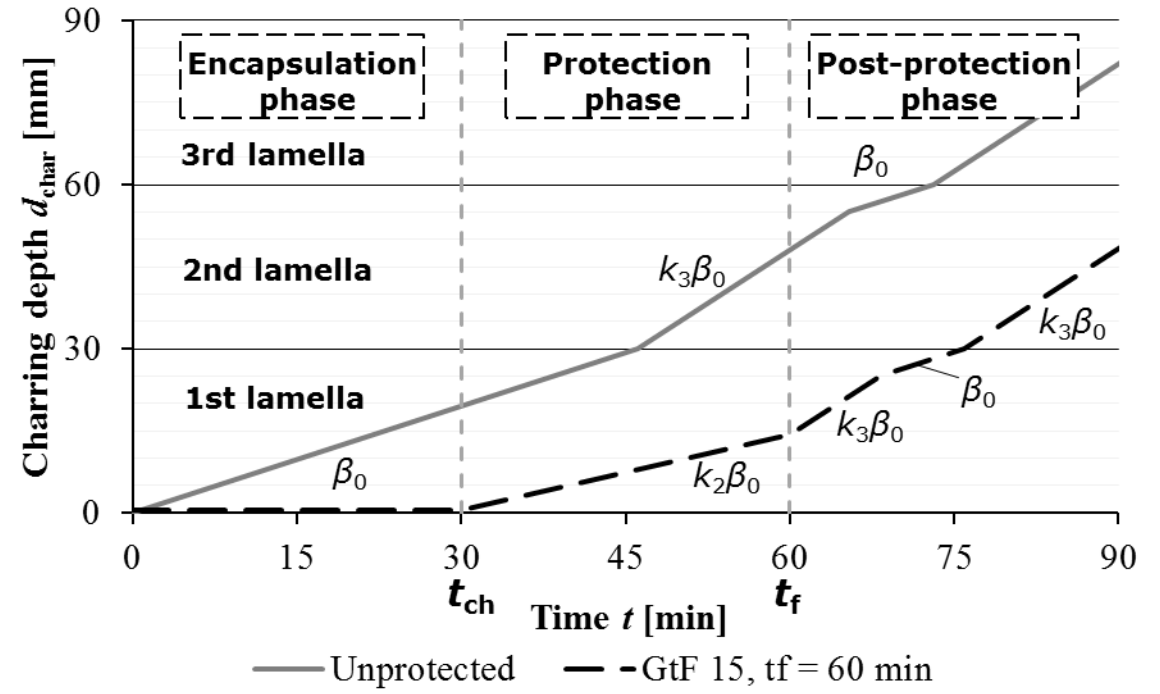
Charring of CLT: Initially protected

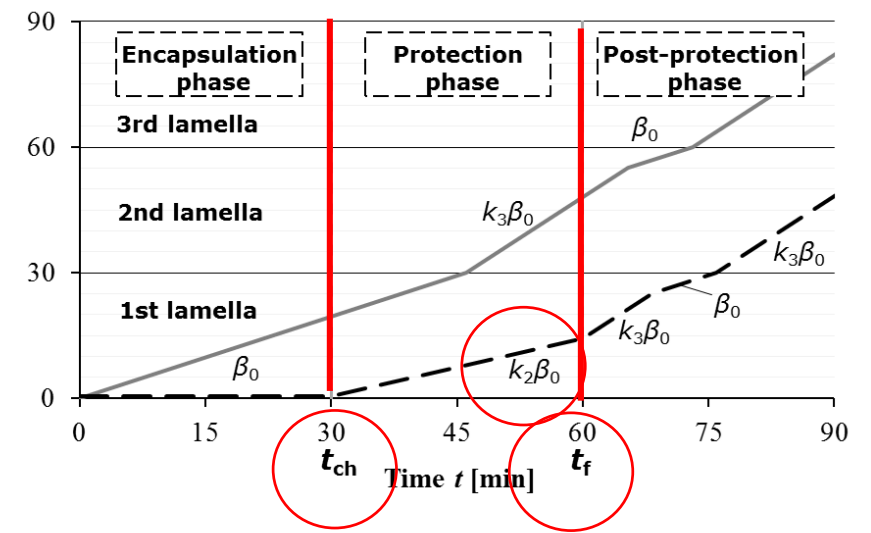


Heat-resistant adhesive



Non-heat-resistant adhesive





$$t_{ch} < t < t_f$$

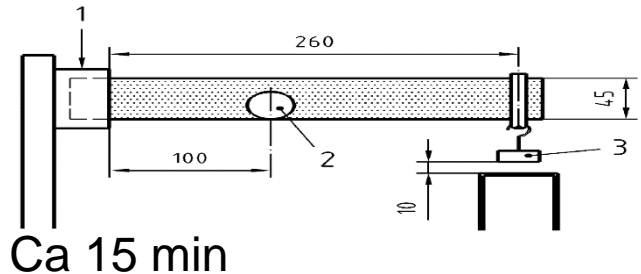
$$t > t_f$$



Gypsum boards



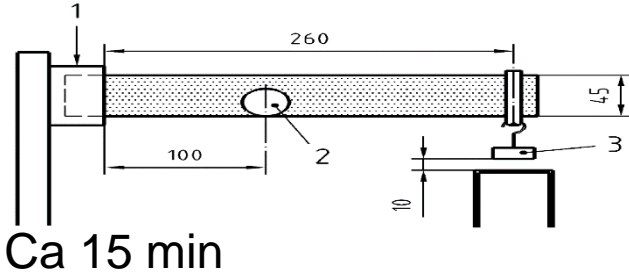
- EN 520



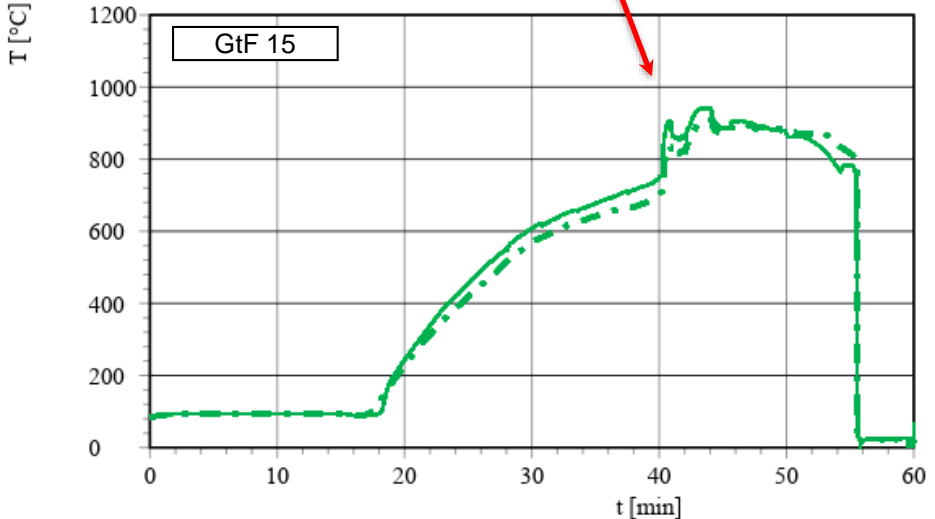
Gypsum boards



- EN 520



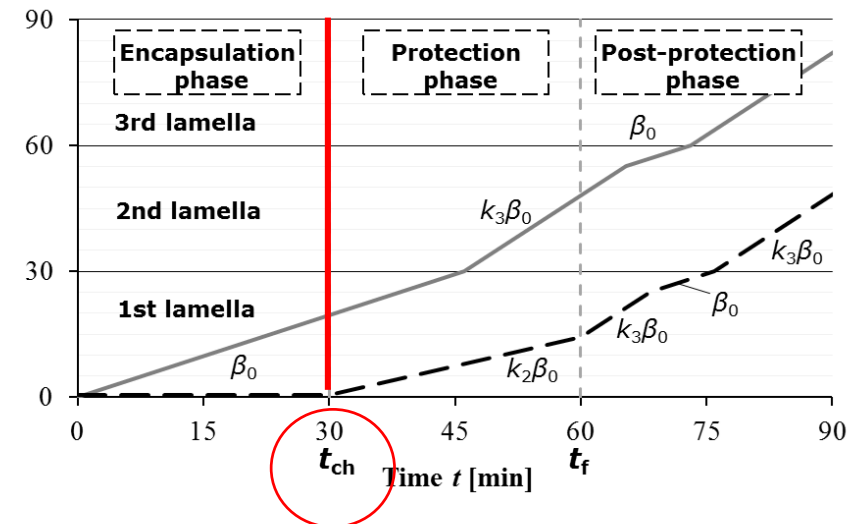
Ca 40 min



Start time of charring behind protection

$$t_{ch}$$

- Tested values for specific products
 - EN 13381-7
- K-classes (EN 13501-2, defined times only!)



SVENSK STANDARD
SS-EN 13381-7:2019

Fastställt/Approved: 2019-07-02
Utgåva/Edition: 1
Språk/Language: engelska/English
ICS: 13.220.50.91.090.20

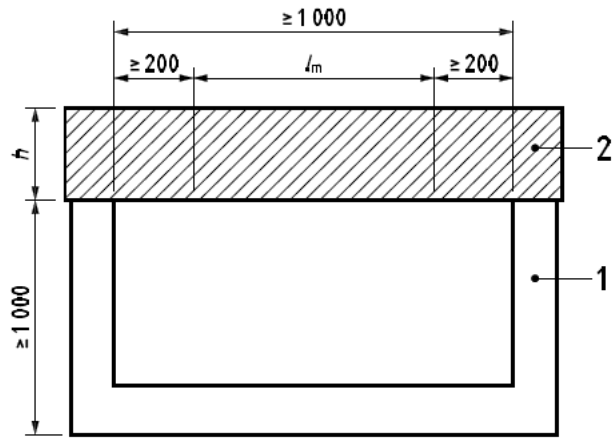
Brandteknisk provning av byggnadsdelar – Bidrag till
brandmotstånd –
Del 7: Skydd av träkonstruktioner

Test methods for determining the contribution to the fire
resistance of structural members –
Part 7: Applied protection to timber members

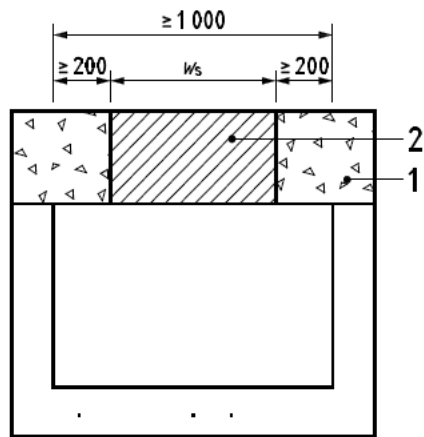


EN 13381-7:2019

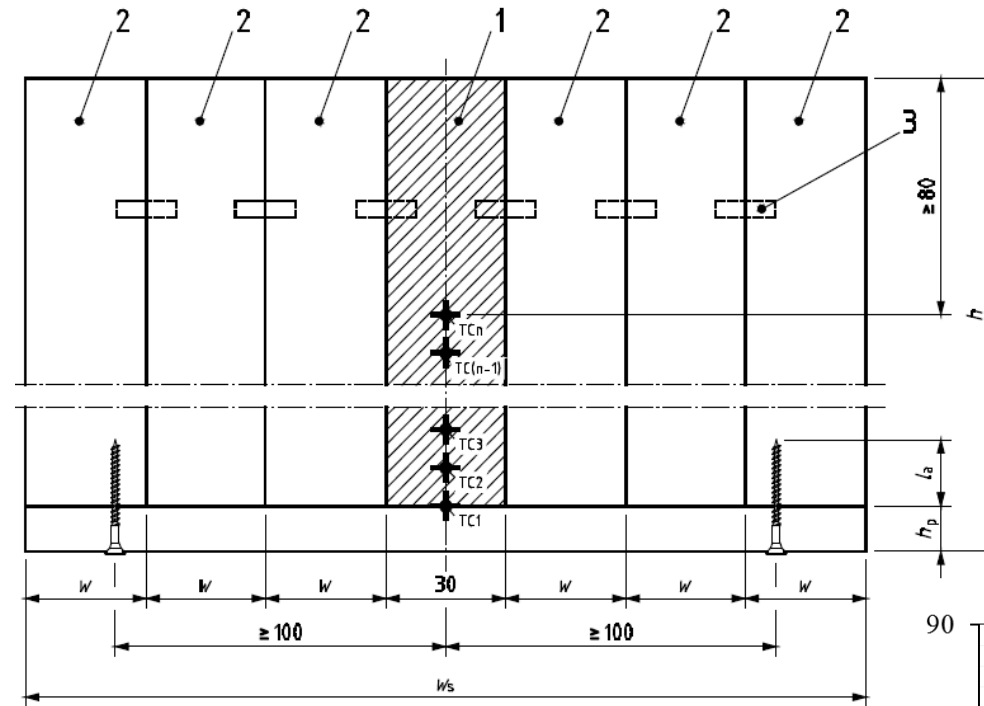
Model scale test



a) Side elevation

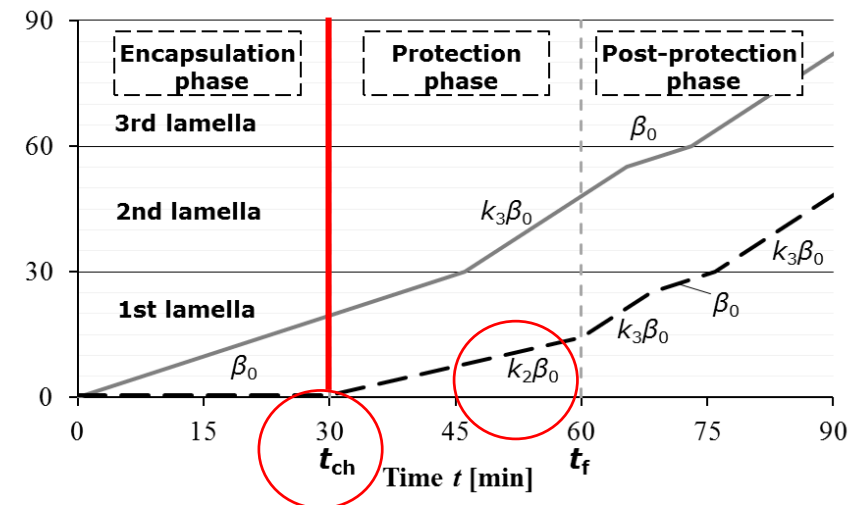


b) End elevation



- y instrumented timber beam (centre beam)
- side timber beams
- w wood dowels (optional)
- depth of the charring specimen
- thickness of the fire protection system
- anchorage length of the mechanical fixation in wood at $t = 0$

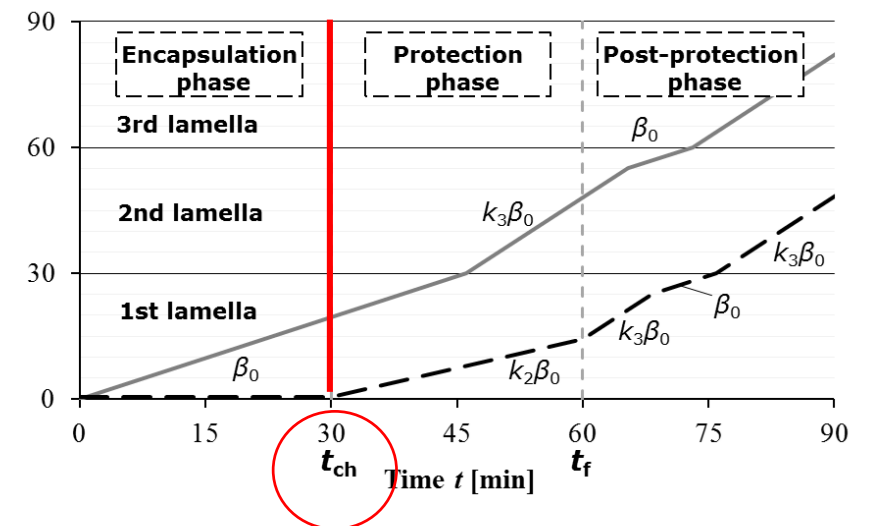
Start time of charring (t_{ch}) and charring rate (k_2)



Start time of charring behind protection

t_{ch}

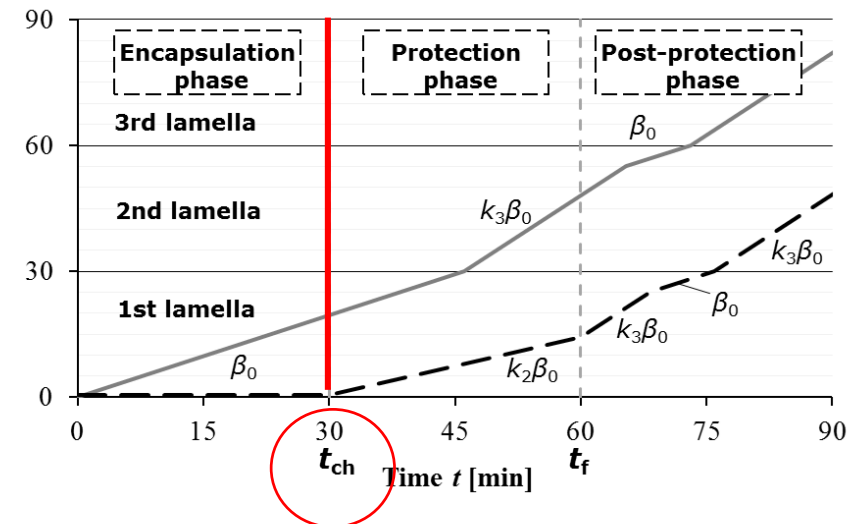
- Tested values for specific products
 - EN 13381-7



Start time of charring behind protection

t_{ch}

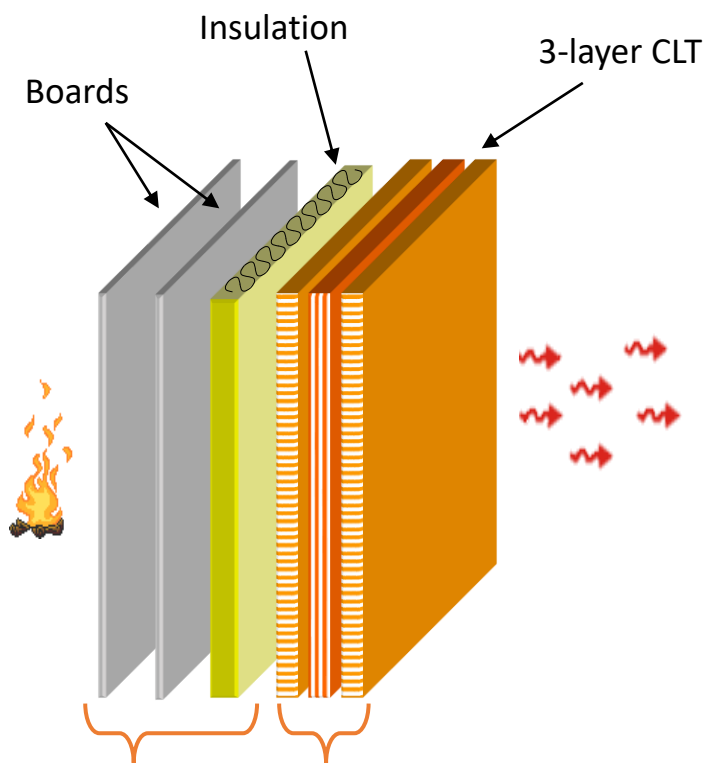
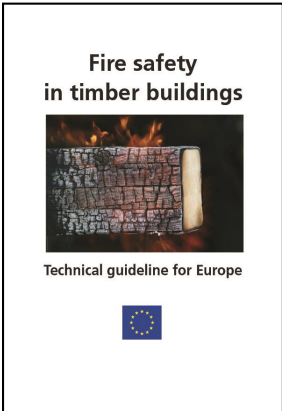
- Tested values for specific products
 - EN 13381-7
 - K-classes (EN 13501-2, strict!)
- Generic values
 - EN 1995-1-2:2004
 - **EN 1995-1-2:2022 (coming soon)**
 - **Sum of protection times**



Separating
Function Method

Calculations

$$t_{ch} = \sum t_{prot, cladding}$$



Fire protection system
 $T_{prot} = 270^{\circ}\text{C}$

Initially protected CLT
 $T_{ch} = 300^{\circ}\text{C}$

$$t_{prot,i} = (t_{prot,0,i} \cdot k_{pos,exp,i} \cdot k_{pos,unexp,i} + \Delta t_i) \cdot k_{j,i}$$

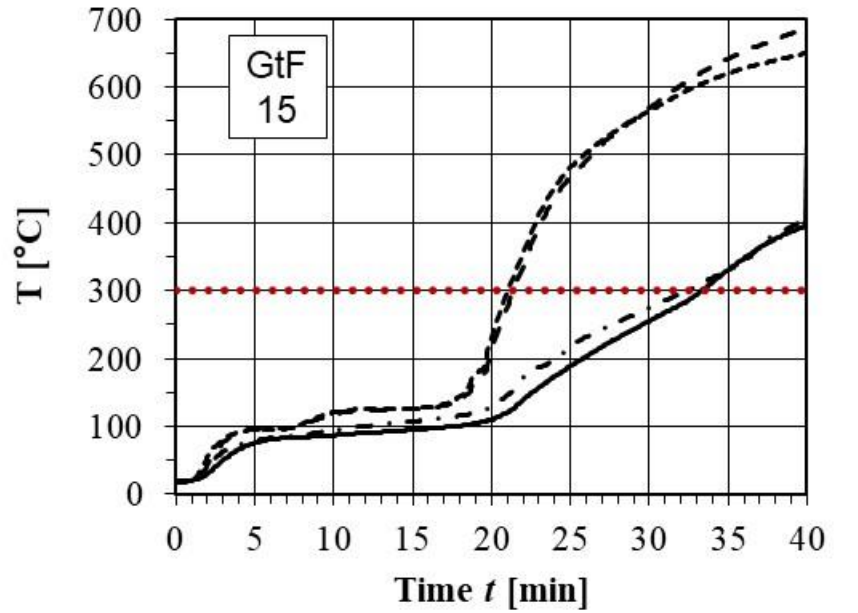
| No | Material | Protection time $t_{prot,i}$ | Sum of protection times |
|----|-----------------------------------|------------------------------|-------------------------|
| | | min | min |
| 1 | Gypsum plaster-board type F (GtF) | 30 | 30 |
| 2 | Gypsum plaster-board type F (GtF) | 11,3 | 41,3 |
| 3 | Stone wool (SW) | 28,7 | 69,9 |
| 4 | CLT | | |

$$t_{ch} = \min \left\{ \begin{array}{l} \sum t_{prot} \\ t_f \end{array} \right.$$

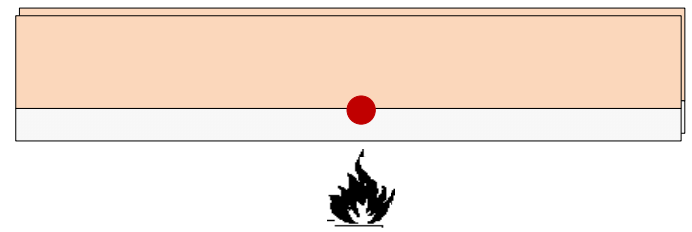
Separating
Function Method

Start time of charring Mineral wool vs wood substrate

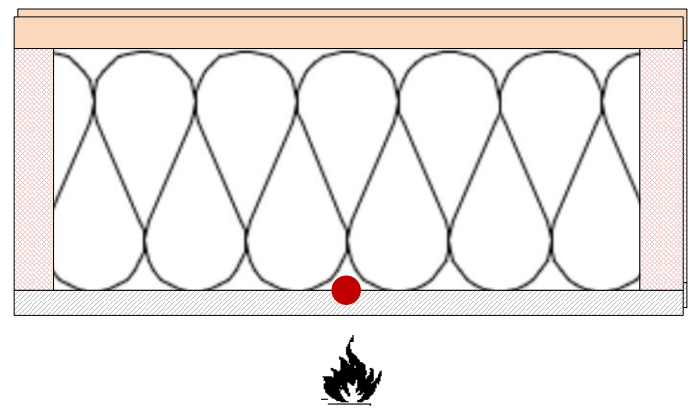
$$t_{\text{prot}} = t_{\text{prot},0} * k_{\text{pos,unexp}}$$



— GtF+wood - - - - GtF + stone wool 45
 - - - GtF+ stone wool 195 - · - · - GtF+GtF
 ····· charring start



$$k_{\text{pos,unexp}} = 1$$

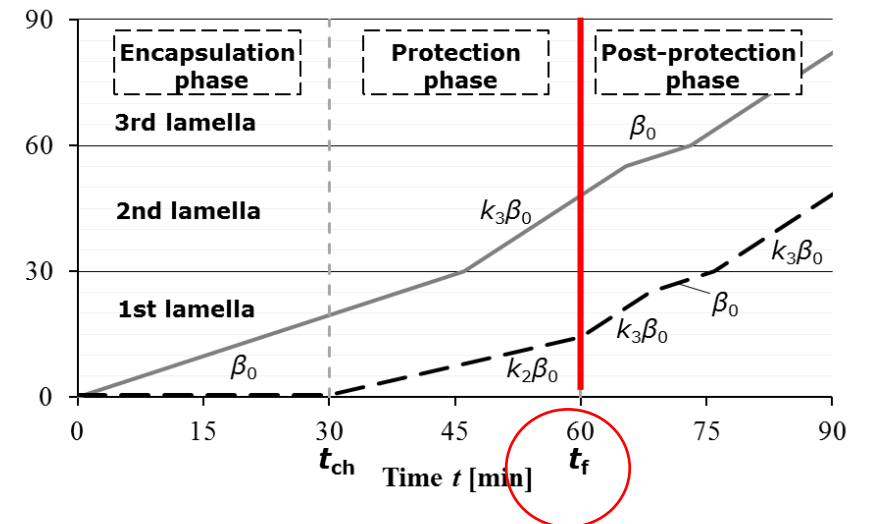


$$k_{\text{pos,unexp}} < 1$$

Failure of the cladding

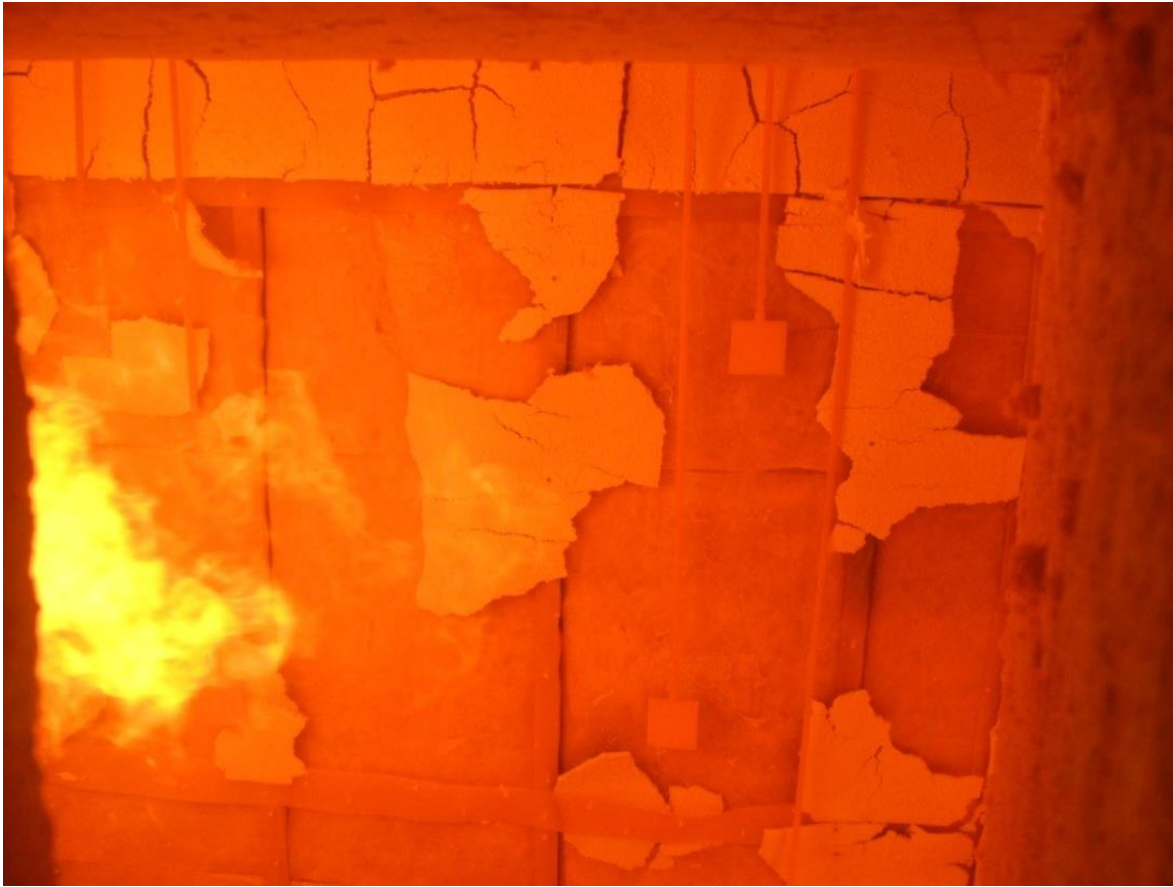
Mechanical degradation

Pull-out of fasteners



Failure time of fire protection system

t_f



Fall-off



Heavy shrinkage

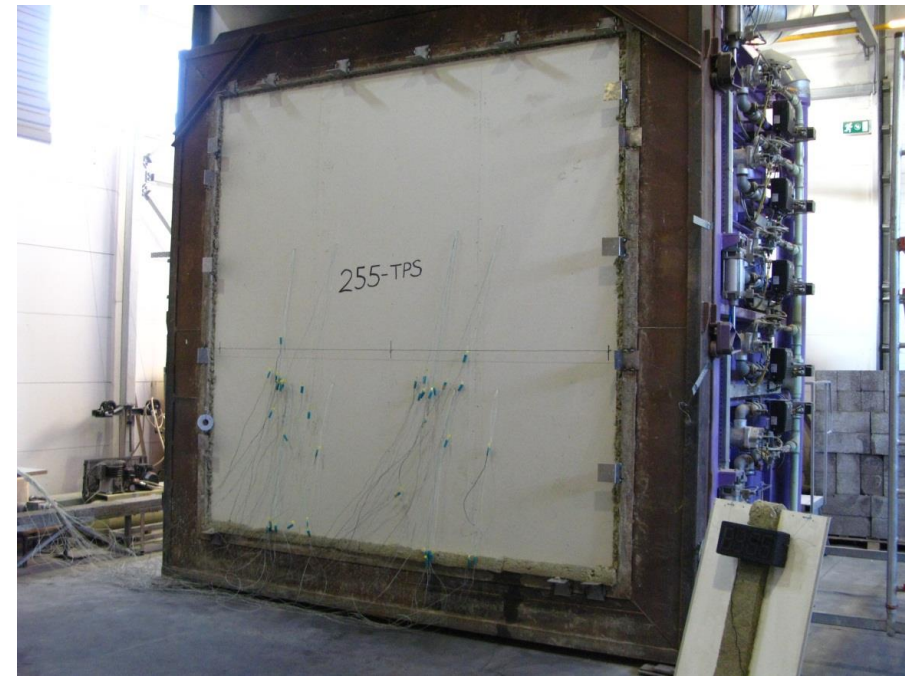
Failure time of fire protection system

t_f

- Tested values for specific products
 - **EN 13381-7:2019**
 - EN 1363, 1364, 1365 series

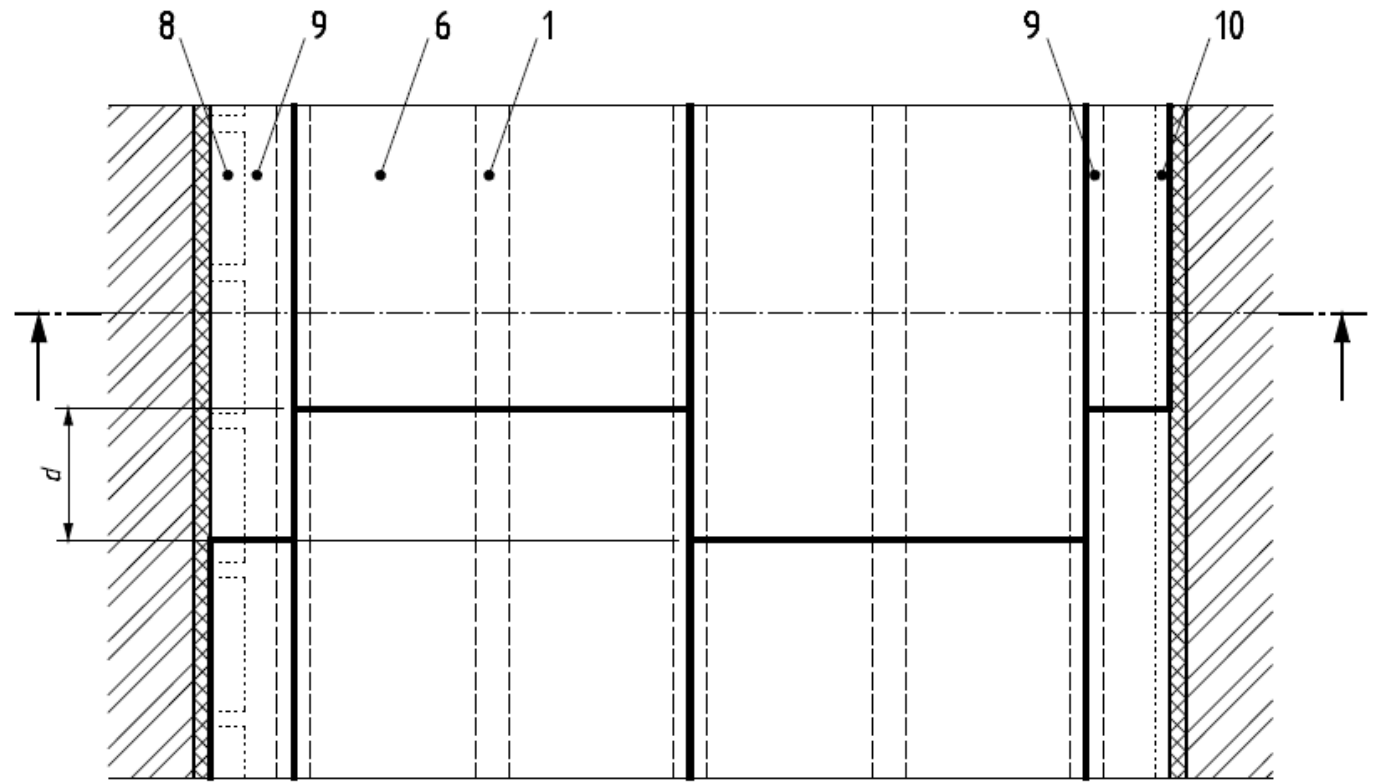
Controlled by TC-s

Visual observations

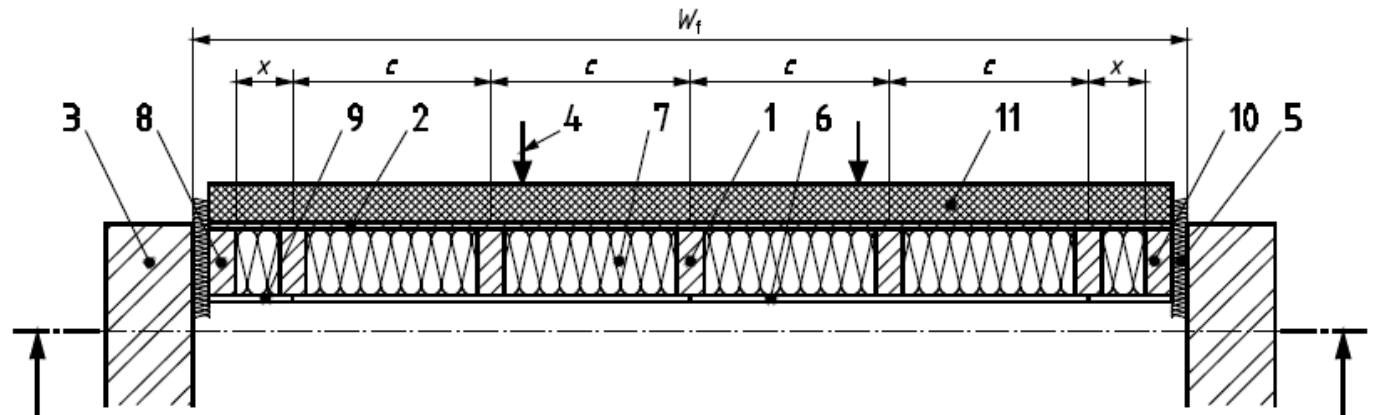


EN 13381-7:2019

Full scale test of a floor



a) Top elevation



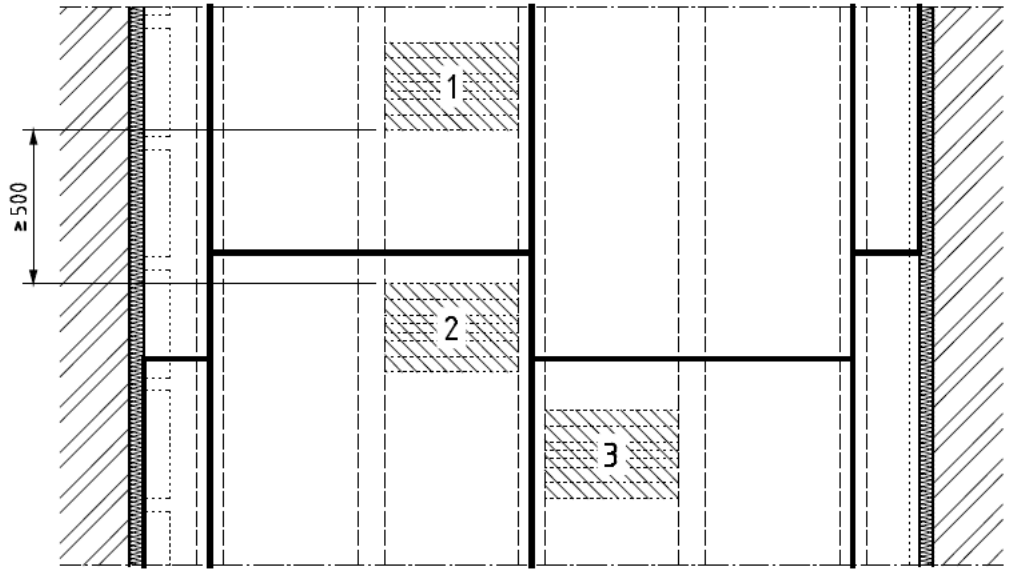
b) End elevation

Key

- | | | | |
|---|-------------------------|-----|--------------------------------------|
| 1 | timber joist | 7 | cavity insulation |
| 2 | decking | 8 | outer joist (example: cut) |
| 3 | furnace | 9 | fire protection board (fitting part) |
| 4 | load | 10 | outer joist (example: half width) |
| 5 | insulation fitting part | 11 | spreader beam |
| 6 | fire protection board | d | board displacement |

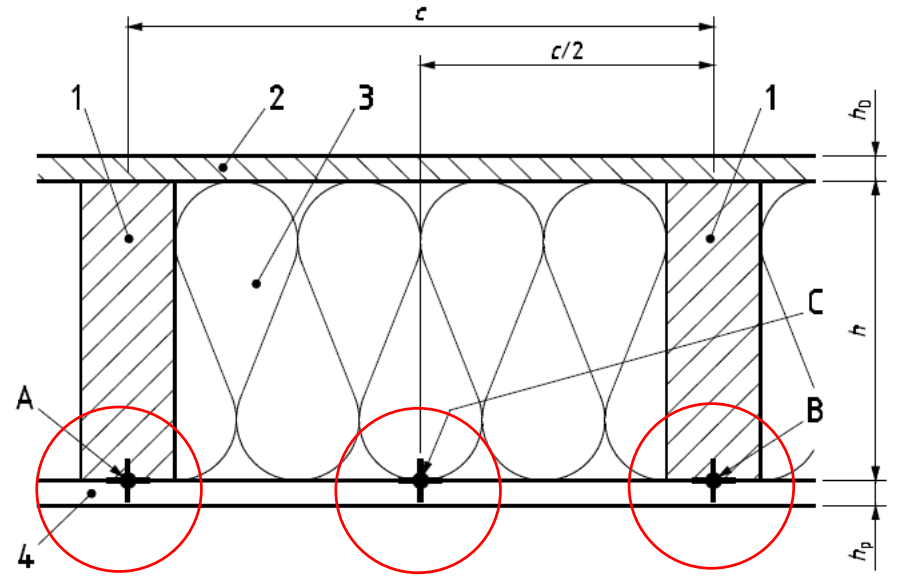
EN 13381-7:2019

Temperature and charring measurements



- Key**
- 1 charring specimen I
 - 2 charring specimen II
 - 3 charring specimen III

Failure time of protection

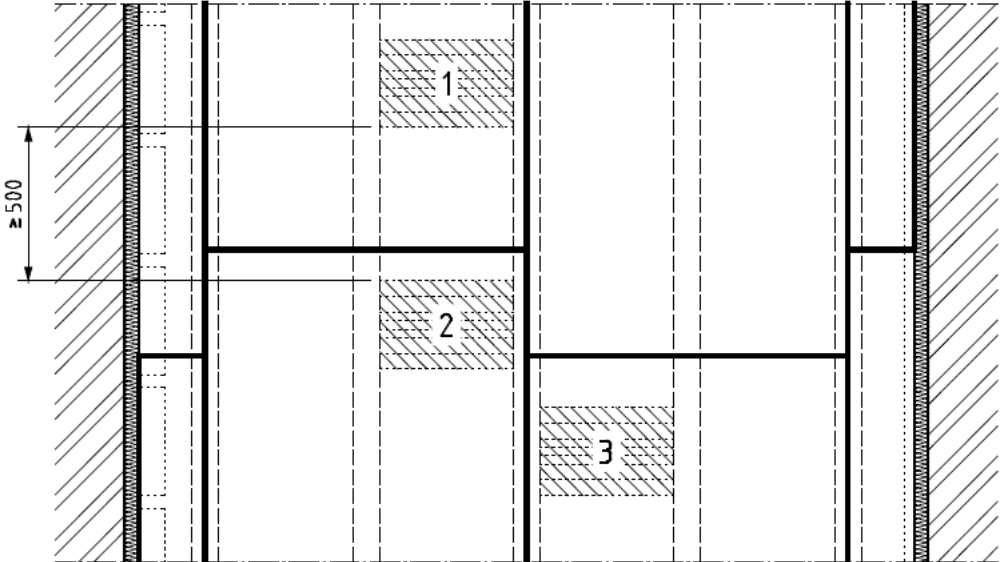


End elevation

- Key**
- 1 loaded joist or stud
 - 2 decking at the non-exposed side
 - 3 cavity insulation (stone wool)
 - 4 fire protection system including joints
 - c centre distance
 - h_p thickness of the fire protection system
 - h_D thickness of the Decking
 - A thermocouple group A: behind the fire protection system more than 200 mm away from any joint
 - B thermocouple group B: behind the fire protection system behind joints (for fire protection systems including joints)
 - C thermocouple group C: Centric between two loaded joists or studs

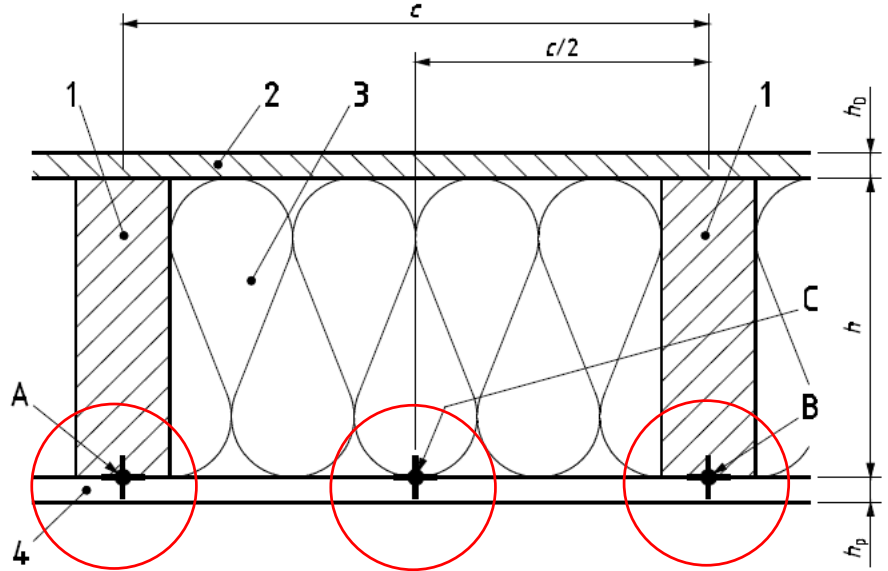
Centre distance of thermocouples 300 mm

Temperature and charring measurements



- Key
- 1 charring specimen I
 - 2 charring specimen II
 - 3 charring specimen III

Failure time of protection



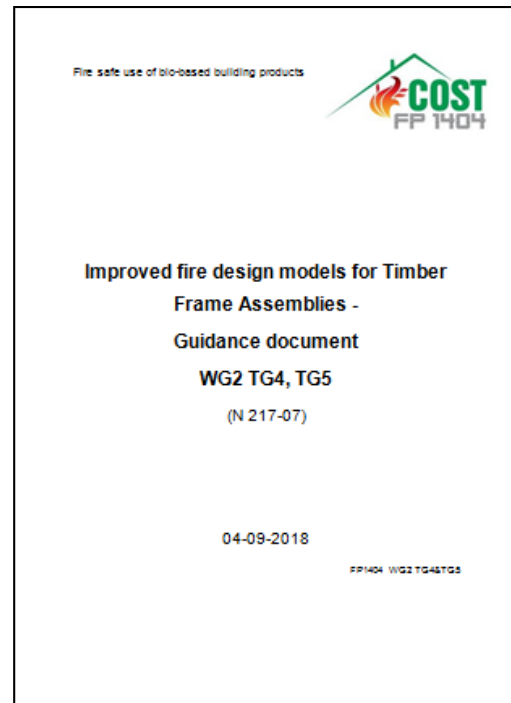
- The failure time:
- Maximum temperature at TC A and TC B; TC C deviates less than 50K from the mean furnace temperature
 - Observations detect loss of stickability in total more than 0,25 m²

Failure time of fire protection system

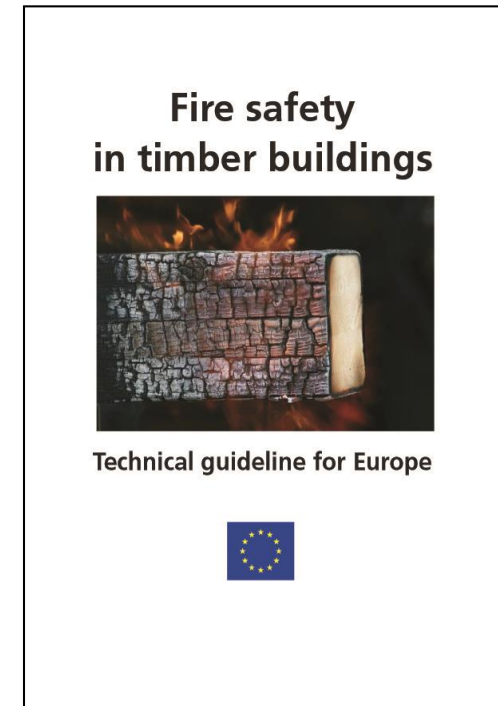
t_f

- Tested values for specific products
 - EN 13381-7:2019 Controlled by TC-s
 - EN 1363, 1364, 1365 series Visual observations
- Generic values
 - Fire Safety in Timber Buildings – Technical Guideline for Europe (2010)
 - COST FP1404 documents (2018)
 - EN 1995-1-2:2022 (coming soon)

*Just et al. (2018)
Improved fire design
models for Timber Frame
Assemblies - Guidance
document N 217-07*



*Östman et al. (2010)
Fire Safety in Timber
Buildings. Technical
guideline for Europe.*



<https://costfp1404.ethz.ch/publications.html>

EN 1995-1-2:20xx

Failure times of gypsum plasterboards

Draft EN 1995-1-2:2022

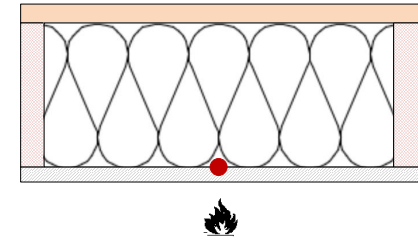


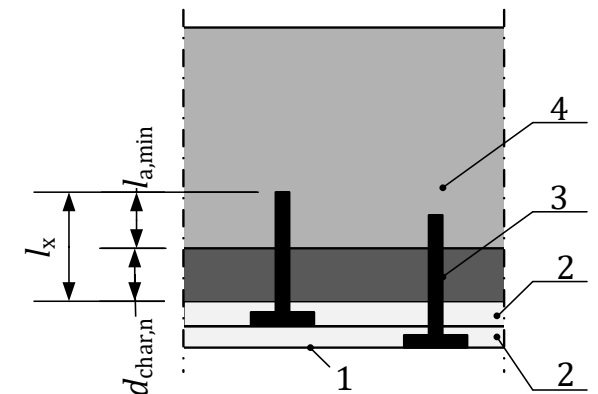
Table 5.9 – Failure time of the fire protection system due to mechanical degradation

| Panel(s) | Walls | | Floors | |
|--|--|-----------------------|--------------------------------|-------------------------|
| | t_f [min] | h_p [mm] | t_f [min] | h_p [mm] |
| Gypsum plasterboards Type F (EN 520), one layer | $4.9 \cdot h_p - 30$ (0.1) | $9 \leq h_p \leq 18$ | $1.6 \cdot h_p + 3$ (0.2) | $12.5 \leq h_p \leq 16$ |
| | 58 | $h_p > 18$ | 29 | $h_p > 16$ |
| Gypsum plasterboards Type F (EN 520), two layers | $1.6 \cdot h_p + 18$ (0.3) | $25 \leq h_p \leq 31$ | $1.9 \cdot h_p - 1.5$ (0.4) | $25 \leq h_p \leq 31$ |
| | 68 | $h_p > 31$ | 57 | $h_p > 31$ |
| Gypsum fibreboards (EN 15283-2) | Values to be included in the second draft if available. | | | |
| where: | | | | |
| t_f | is the failure time of the fire protection system due to mechanical degradation, in min; | | | |
| h_p | is the thickness of the fire protection system; in mm. | | | |

Failure time due to pull-out of fasteners

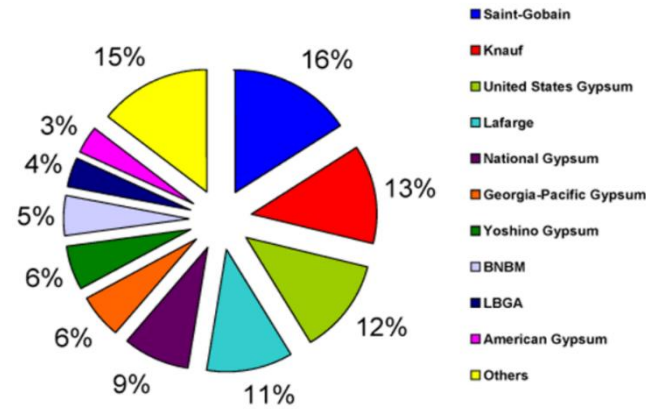
$$t_f = t_{ch} + \frac{l_x - l_{a,min}}{\beta_n}$$

For gypsum plasterboards, Type A
 $t_f = t_{ch}$

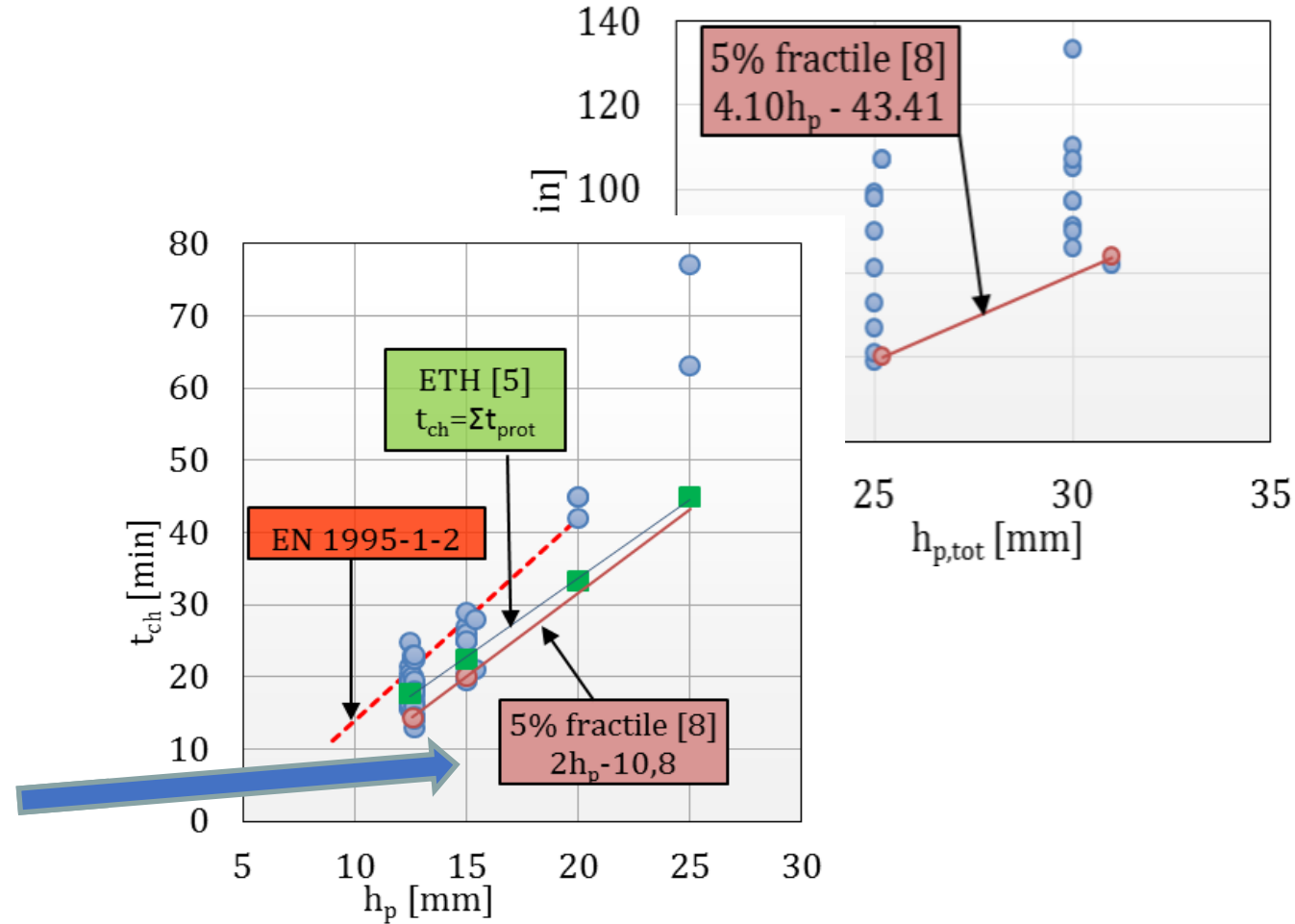
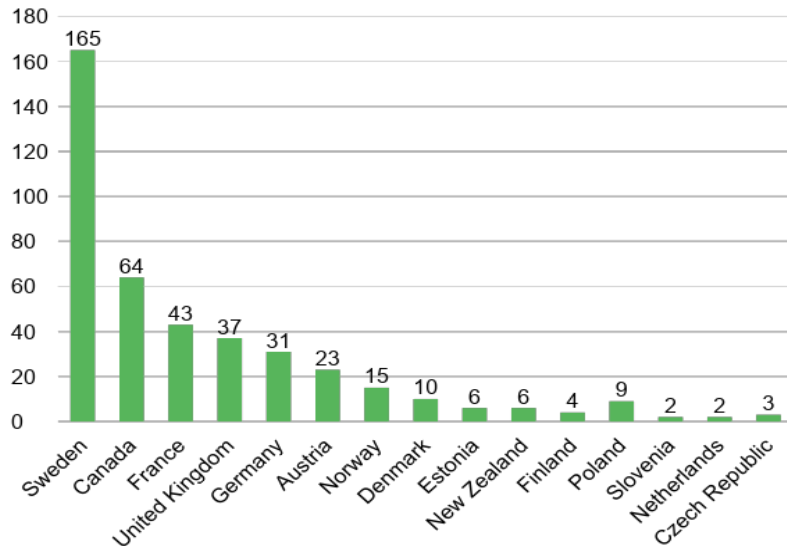


Analysis of the database

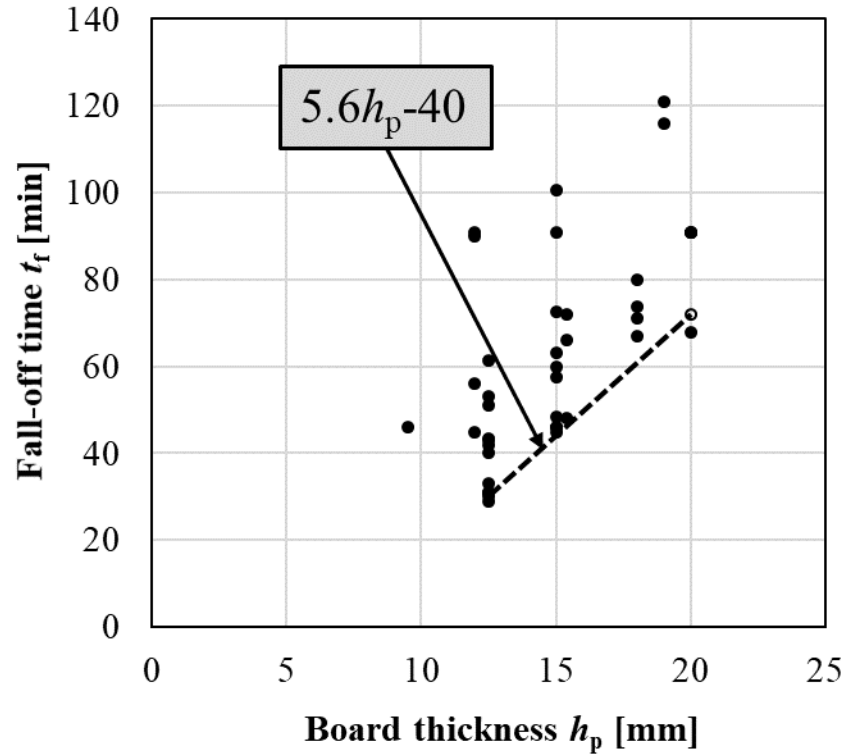
- Held at RISE Research Institutes of Sweden
- 470 full scale test reports



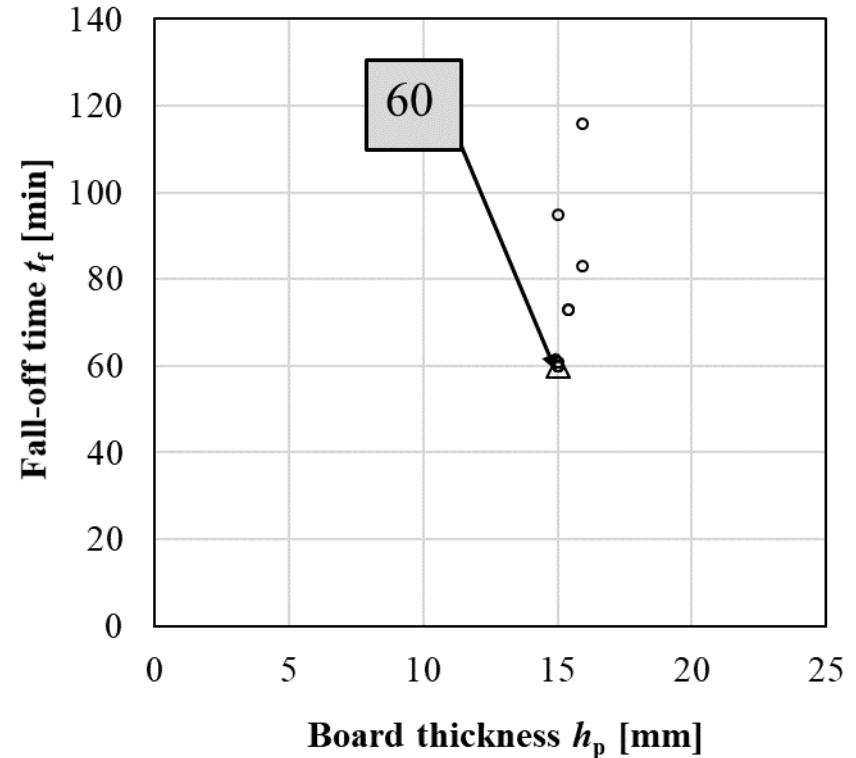
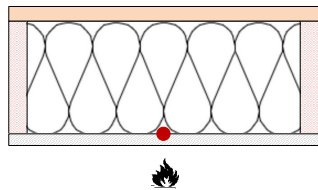
Full scale fire test reports



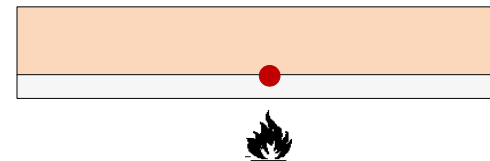
Effect of substrate



Gypsum plasterboards on **insulation**



Gypsum plasterboards on **CLT structures**



Effect of fastening on failure time

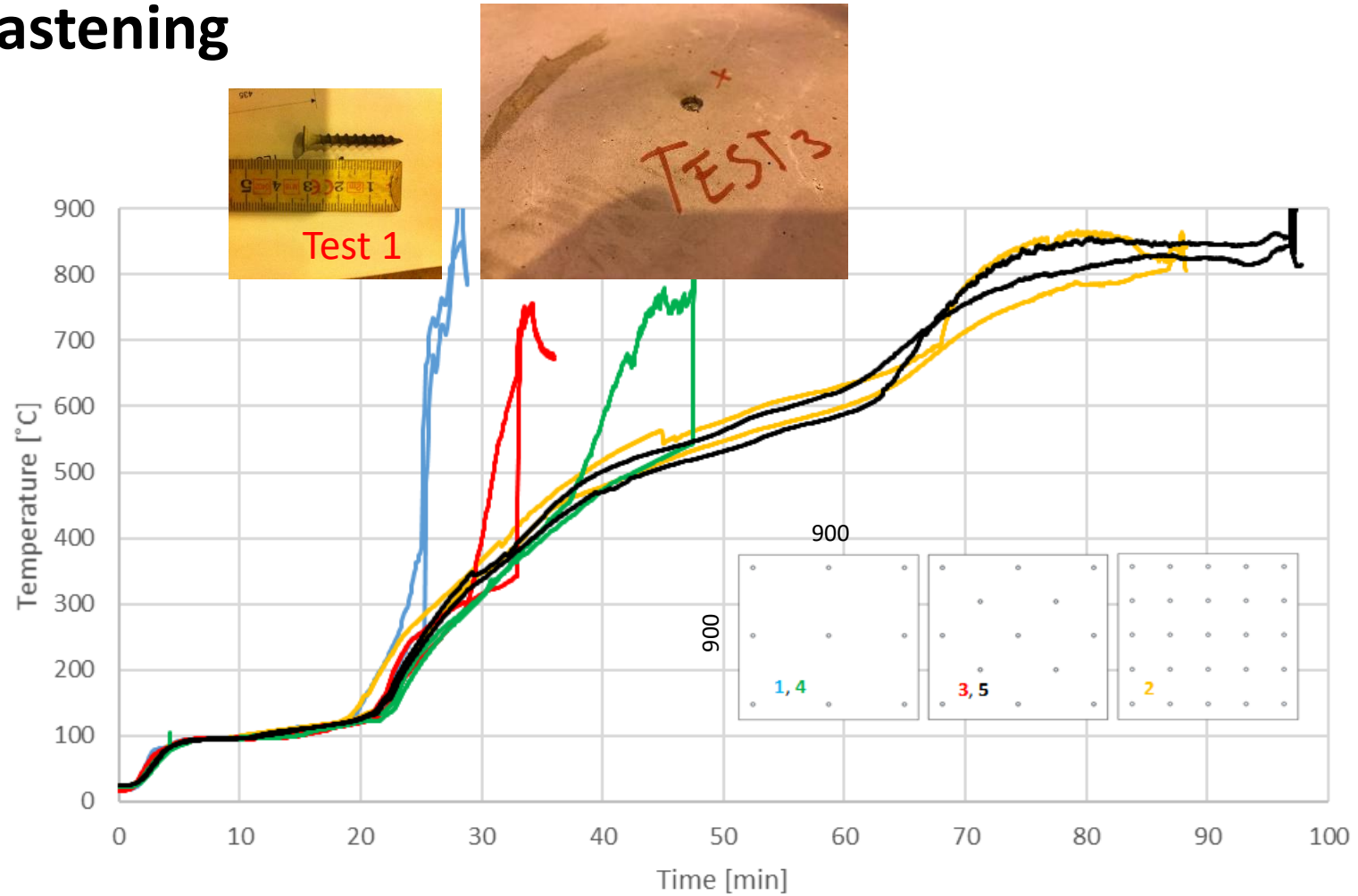
- Studs or beam spacing
- Spacing of fasteners
- Quality of mounting

120 min

Gypsum plasterboard,
Type F 15 mm



Effect of fastening



Model scale tests
GtF 15 on CLT

— TEST 1 — TEST 1 — TEST 2 — TEST 2 — TEST 3
 — TEST 3 — TEST 4 — TEST 4 — TEST 5 — TEST 5

Summary

- Different charring phases for initially protected structures depending on properties of protection system.
- Substrate and fastening can influence start time of charring and failure time significantly.
- Start time of charring and failure time can be determined by EN 13381-7
- Generic values on start time of charring calculated according to Separating Function Method
- Generic values of failure times for gypsum boards in EN 1995-1-2:2022.



THANK YOU FOR
YOUR ATTENTION!

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